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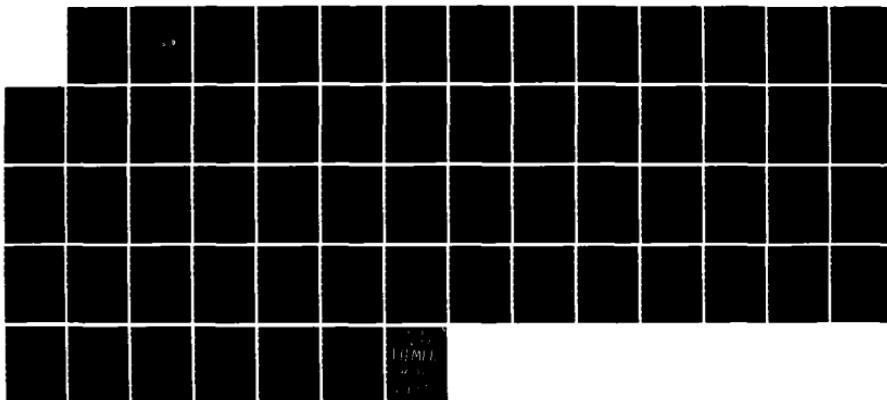
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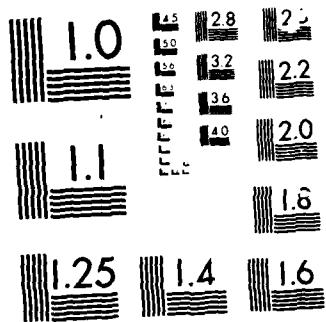
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COMBINED DIRECT/INVERSE THREE DIMENSIONAL TRANSONIC WING
DESIGN WITH VISCOUS AND WING/BODY EFFECTS

VOLUME 2 : USERS GUIDE FOR ANALYSIS/DESIGN COMPUTER PROGRAM

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ABSTRACT

This users guide describes the input and operation requirements of a computer code for the analysis and design of wings in transonic flow. A synopsis of the function of the major subroutines in the program is given in addition to a detailed description of the input variables required to run the code. Sample data sets are presented that illustrate the data sequence required for various code options.

ADMINISTRATIVE INFORMATION

The work presented was a joint effort by Lockheed-Georgia Company and Texas A&M University supported by the Naval Air Systems Command under the cognizance of D. G. Kirkpatrick (NAVAIR-311D AIRTASK WR02302), Navy Contract N00167-81-C-0078-P00004. The authors acknowledges the support of Dr. Tsze C. Tai, contract monitor at David Taylor Ship/Research and Development Center during all phases of this research.

INTRODUCTION

This users guide describes the inputs required to run the Lockheed-Georgia Direct/Inverse Design Code (ZEBINV) in the analysis and design modes. The following sections include a brief description of how the code works, a detailed description of the required input data, along with sample input decks and an example of the typical output from the code.

DESCRIPTION OF CODE OPERATION

In the analysis mode, the Lockheed Georgia Direct/Inverse Design Code (ZEBINV) computes the inviscid potential flow about three-dimensional wings using the ZEBRA II algorithm developed by South et al. The conservative full potential equation is solved on a stretched Cartesian grid that is sheared to align with the leading and trailing edges of the wing.

A typical analysis run begins with the inputting of data that define the airfoil geometry at different spanwise control stations, the wing planform geometry, mesh generation parameters, flow solver initialization and control

parameters. Subroutines SECTIN and INPUT control the reading in of all analysis data. After the required data has been input, the program calls routines to generate the computational grid (SETUP) and compute initial flow parameters (INIT). Subroutine ZEBRA is then called to generate the potential flow solution. ZEBRA calls subroutine WNGBC2 to compute and update both wing surface and outer grid boundary condition, subroutine RO to compute the density at grid half points, and subroutine ROCOZ to compute the retarded density coefficients used in the potential flow solver. Subroutine OUTPUT is called at the end of the solution to compute and print output parameters.

When viscous analysis or design is selected, subroutine VISACT is called from ZEBRA to compute the displacement thickness due to the boundary layer and to update the surface boundary conditions to account for the viscous effects. A second viscous flow routine BDLY is called to compute viscous effects during inverse design cases.

Wing/body effects are computed in subroutine WONZ which is called by INIT. WONZ is called prior to the start of the potential flow solution for each grid of a grid sequencing run.

During inverse design cases, two subroutines are called to compute the current wing shape and perform a wing reloft to enforce a desired trailing edge thickness. These subroutines are SHAPE and RELOFT. When relofting is in effect SHAPE is called by RELOFT. RELOFT is called from subroutine ZEBRA at a specified iteration frequency.

The sequencing of the input routines, flow solver, and output routines is controlled by the main program ZEBINV. This program contains logic that allows grid sequencing to be used to speed up the flow solution. The sample data sets presented in the following sections illustrate the use of a sequence of three grids in the flow solution.

DETAILED DESCRIPTION OF INPUT

The input data set required by the analysis/design code can be

broken into five distinct types of data. These data types are:

1. Airfoil section ordinates at specified span locations
2. Data to define the wing planform
3. Control parameters for mesh generation and solution initial
4. Wing/Body data
5. Inverse design data

Each different type of data will be described separately. The input be described card by card. This description will contain both definition of the input variable and the input format.

A. Airfoil Section Inputs and Test Case Title

Section ordinates can be defined at up to 11 span locations of the airfoil section ordinates are:

1. TITLE1, TITLE2, ATITLE (3 cards, 8A10)

TITLE1 - Two card test case title and description that

TITLE2 is written to output files.

ATITLE - Airfoil data description.

2. NPAN, INU, INL, KSMTHS (1 card, 8I10)

NPAN - Number of span stations at which airfoil ordinates are to be defined - at least two stations are required (2.LE.NPAN.LE.11)

INU = Number of upper surface airfoil ordinates. Must be the same for all sections .LE. 100.

INL = Number of lower surface airfoil ordinates. Must be

the same for all sections .LE. 100.

KSMTHS = Number of times computed surface slopes are smoothed.

3. XINU(I), I = 1, INU (INU/8 Cards, 8F10.0) x/c at which airfoil upper surface ordinates are input for the wing section.

4. XINL(I), I = 1, INL (INL/8 Cards, 8F10.0) x/c at which airfoil lower surface ordinates are input for the wing section.

5. ZUP(I, 1), I = 1, INU (INU/8 Cards, 8F10.0) upper surface airfoil ordinates (Z/C) at wing root.

6. ZLP(I, 1) I = 1, INL (INL/8 Cards, 8F10.0) lower surface airfoil ordinates at the wing root station.

The airfoil sections at span stations 2 through NPAN are defined by the following sequence of cards.

7. ISAMX, ISAMZ (1 Card, 2L5).

ISAMX = T ordinates will be defined at the x/c locations of the root section.

= F new x/c locations will be input. The corresponding z/c ordinates will then be splined onto the root X/C locations.

ISAMZ = T use ordinates for previously defined station.
= F input new z/c ordinates.

8. If ISAMX = T AND ISAMZ = F, repeat cards 5 and 6 after 7.

9. If ISAMX = F and ISAMZ = F, repeat cards 3 through 6 after card 7.

10. To use airfoil section defined at station N-1 at station N,
repeat card 7 with ISAMX = T and ISAMZ = T.

Planform Geometry

1. Header (2X)

2. PTITLE (1 Card, 8A10)

80 character wing planform description

3. YROOT, XLER, XTER, YTIP, XLET, XTET, SREF, CREF, XMON (2
Cards, 6F10.0)

These variables define trapezoidal reference wing:

YROOT = Y coordinate of root
XLER = X coordinate of L.E. at root
XTER = X coordinate of T.E. at root
YTIP = Y coordinate of tip
XLET = X coordinate of L.E. at tip
XTET = X coordinate of T.E. at tip
SREF = Wing reference area (Semi Span Area)
CREF = Reference chord
XMON = Moment reference

4. NLES (1 Card, 8I10)

NLES - Number of segments input to describe the leading
edge (NLES.LE.3).

5. NLEI (1 Card, 8I10)

NLEI = Number of Y,X pairs defining leading edge
(NLEI.LE.10).

6. YLEI(I),XLEI(I),I=1,NLEI (NLEI/4 Cards, 8F10.0)

YLEI,XLEI = Y,X pairs defining the leading edge segment

At least two pairs required.

Same dimensional system as XLER, etc.

7. DXLER,DXLET (1 Card, 8F10.0).

DXLER = DX/DY of L.E. at inboard edge of segment

DXLET = DX/DY of L.E. at outboard edge of segment

Note: Repeat cards 5 through 7 NLES times

8. NTES (1 Card, 8I10)

NTES = Number of segments input to describe the trailing edge (NTES.LE.3)

9. NTEI (1 Card, 8I10)

NTEI = Number of Y,X pairs defining trailing edge segment
(NTEI.LE.10).

10. YTEI(I),XTEI(I),I=1,NTEI (NTEI/4 Cards, 8F10.0)

YTEI,XTEI = Y,X pairs defining the trailing edge segment

At least two pairs required

11. DXTER,DXTET (1 Card, 8F10.0)

DXTER = DX/DY of T.E. at inboard edge of segment

DXTET = DX/DY of T.E. at outboard edge of segment

NOTE: Repeat cards 9 through 11 NTES times

12. YP(N),THETP(N),N=1,NPAN (NPAN/4 Cards, 8F10.0)

YP = Fraction of semispan at which airfoils are defined

THETP = Twist Angle, degrees, at YP - Positive if leading edge is up

C. Mesh Generation and Solution Parameters

A set of five namelists are used to input values that control mesh generation, solution initialization and solution sequencing. Namelist GPARM, XGRID, YGRID, and ZGRID are used in mesh generation. Namelist SOLVIN is used to put flow solver parameters. A sixth namelist VISCDT is input after SOLVIN if IVISC = 1 in SOLVIN. This set of namelists must be input for each grid in a grid sequencing run; however, only those values that change from grid to grid must be redefined. The namelists and the input parameters required for analysis runs are:

1. TITLEM (1 Card, 8A10)

Namelist set description

2. GPARM (Namelist input - Default values in parenthesis)

IPRNTG = 1 - Prints computational grid (0)

WBCPRT = .T. - Prints upper and lower surface slopes at each spanwise grid station (.F.)

NTIPEL = 1 - Generates a constant chord tip extension with tip section sweep from wing tip to outer boundary

3. XGRID (Namelist input)

NXON - Number of streamwise mesh points on wing surface at each span station

NXFWD- Number of streamwise mesh points ahead of the wing leading edge

NXAFT- Number of streamwise mesh points aft of the wing trailing edge

XPLE - Grid stretching factor for grid in front of wing; computed in MESHZ for XFWD .NE.0

XPTE - Grid stretching factor for grid behind wing; computed in MESHZ for XAFT .NE.0

XFWD - Desired location of the upstream boundary referenced to the leading edge of the wing (in root chords).

XAFT - Desired location of the downstream boundary referenced to the leading edge of the wing (in root chords).

4. YGRID (Namelist input)

NYON - Number of spanwise grid points on wing surface

NYOFF- Number of spanwise grid points off of the wing surface

YPTIP- Grid stretching factor for grid beyond wing tip, computed in MESHZ when YMAX .NE.0

YMAX - Desired location of the spanwise outer boundary referenced to the wing tip (in semi-spans). For example, YMAX=1.3 places the spanwise boundary at 1.3 semi-spans beyond the wing tip.

5. ZGRID (Namelist input)

NZ - Number of vertical grid points

ZP - Grid stretching factor for vertical direction. The grid is stretched equally above and below the z = 0 plane.
Computed in MESHZ when ZMAX .NE. 0

ZMAX - Desired location of the top and bottom boundaries of the computational plane (in root chords).

6. SOLVIN (Namelist input)

MACH - Free-stream Mach number for test case

AOA - Wing angle of attack in degrees

OMEGX

OMEGY- Relaxation parameters for the x, y, and z directions
OMEGZ

OMEGG- Relaxation factor for circulation

MAXIT- Maximum number of iterations of the flow solver

RCONV- Convergence tolerance = the ratio of current maximum residual and initial residual

NGSEQ- Number of grids to be used in grid sequencing runs

IPRINT = 1 - Calls output to print flow solution parameters

I PLOT = 1 - Writes plot data to a specified logical unit for post-processing

I VISC = 1 - Selects viscous analysis/design mode

I FUSE = 1 - Turn on wind body effects with circular cylinder fuselage

= 2 - Turn on wing body effects using input fuselage cross-sections

I CIRPF - Spanwise circulation distribution print frequency Prints every ICIRPF iterations

I KLUNK = 1 - Updates outer boundary potentials using Klunkers expressions

= 0 - Sets outer boundary potentials to zero

I PU - Logical unit to which plot data will be written

I INV = 1 - Perform inverse design

I DESN = 1 - Design both upper and lower surfaces

= 2 - Design upper surface only

= 3 - Design lower surface only

I RLOFT = 1 - Start wing relofting for trailing edge closure on initial grid for NGSEQ.NE.0

= 2 - Start wing relofting for trailing edge closure on second grid for NGSEQ.NE.0.

= 3 - Start wing relofting for trailing edge closure on third grid for NGSEQ.NE.0.

NF - Number of fuselage control points used to evaluate wing/body effects (50 or less)

NITRL - Perform NITRL iterations before first wing reloft

NITRF - Reloft wing every NITRF iterations

NJSHP - Print relofted data every NJSHP span stations

NITDSN - Perform NITDSN iterations prior to start of inverse design

ILED - Initial chordwise index to begin inverse design

ITED - Trailing edge index

ISVSHP - Save inverse shapes at end of run

IRSTART - Restart from previous run

ISRLOR - Save relofted ordinates for restart runs

IPRSHP - Print relofted shapes

7. VISCDT (Namelist input) - only if IVISC .NE. 0 in SOLVIN

RN - Reynolds number based on root chord

DELCOR - Square of the cosine of an appropriate sweep angle such as the mid-chord used to modify boundary layer calculation for 3D effects

NVISC - Number of potential flow solver iterations prior to first viscous update

ITR - Updates viscous corrections every ITR iterations after first update

NPRV - Print viscous flow information every NPRV iterations

NJPRV - Print viscous information every NJPRV span stations

XIBDLY - X/C location of transition point for both upper and lower surfaces

XSEP - X/C location before which the separation parameter, SEP, is restricted to a maximum value of 0.004. After XSEP, SEP can have any value

XPCI - Lower surface X/C location after which a decreasing lower surface displacement thickness is forced to continue decreasing

D. Wing/body Data

The format of the wing/body data depends on the value of IFUSE entered in namelist SOLVIN. If IFUSE = 1, the fuselage is simulated by a circular cylinder with elliptic end caps. If IFUSE=2, the cross-sectional areas of the fuselage are input, see sample cases 4 and 5. The wing/body input is performed only once during a grid sequencing run, usually a call to SOLVIN.

The input sequence for the wing/body data is:

1. Header card (1X)
2. XBOD,YBOD,ZBOD,RBOD,TL,ALF (8F10.6)

XBOD - Distance from nose of fuselage to leading edge of wing at the wing root

YBOD - Distance from centerline of the body to the wing root

ZBOD - Distance from centerline of the body to the centerline of the wing (positive is up)

RBOD - Radius of circular cylinder body for IFUSE = 1

TL - Length of the fuselage

ALF - Length of semimajor axis of ellipsoidal ends for IFUSE=1

if IFUSE = 2, input:

3. Header card (1X)

4. NST - Number of cross-sections to be input (I5)

5. XFL(I),AREA(I), I=1,NST (3F10.6)

XLF - % Fuselage length

AREA - Cross-sectional area at XFL

E. Inverse Design Input

When IINV=1 in SOLVIN, the target pressure distribution for the specified span stations must be input. If IDESN=1, the target pressures for both the upper and lower surfaces are input. If IDESN = 2 or 3, the target pressures for either the upper or the lower surface are input. The card sequence for the inverse design input is as follows; see sample data set 6:

1. Header card (1X)

2. JD1,JD2,NCPS (3I5)

JD1 - Index of initial spanwise inverse design station

JD2 - Index of final spanwise design station

NCPS - Number of chordwise points in the target pressure distribution

3. XUD(J,I), I=1,NCPS - Upper surface target Cp X/C locations
(7F10.6)

4. CPDU(J,I), I=1,NCPS - Lower surface target Cp values (7F10.6)

5. XLD(J,I), I=1,NCPS - Lower surface target Cp X/C locations
(7F10.6)

6. CPDL(J,I), I=1,NCPS - Lower surface target Cp values (7F10.6)

Repeat cards 3 through 6 for J=JD1,JD2

Omit cards 5 and 6 for IDESN=2

Omit cards 3 and 4 for IDESN=3

If relofting (IRLOFT .GT. 0) is selected for either viscous or inviscid design cases, the desired trailing edge ordinates of the surface being designed is input after the target pressure data. The card sequence for the relofting data is as follows:

1. Header card (1X)

2. NTE - Number of relofting stations input. This should be equal to the number of design stations (IS)

3. ZUTED(I) ,I=JD1,JD2 - Desired upper surface ordinate of design airfoil. (7F10.0)

4. ZLTED(I) ,I=JD1,JD2 - Desired lower surface ordinate of design

airfoil. (7F10.0)

Omit cards 4 for IDESN=2.

Omit cards 3 for IDESN=3.

DESCRIPTION OF OUTPUT

PRINTED OUTPUT

A typical output will have three sections. In the first section, the parameters that were input to define the wing geometry are echoed. The x location of the wing leading and trailing edges and slope of the leading edge and trailing edge lines at different span stations are printed along with the computed planform geometry parameters such as aspect ratio and taper ratio. These values are normalized by the root chord. The next section of data is generated during the solution process. At the end of each iteration, the iteration number, the grid indicies and values of the maximum correction and residual, the number of supersonic points, the current wing lift coefficient based on circulation and the average residual are printed. If IPRINT = 1 subroutine OUTPUT will be called to compute and print the section lift drag, and moment coefficients and the chordwise upper and lower surface pressure coefficient, density and mach number distributions at each spanwise grid station. A printer plot of the pressure coefficients is also generated.

During inverse runs the relofted shape is printed every NSHPF iterations. If relofting has been selected, the correction to the trailing edge thickness applied at each design station is printed.

When viscous analysis or design is selected, a summary of the boundary layer parameters are printed everyd NPRV updates of the boundary layer for both the upper and lower surfaces of the wing. In addition, a summary of the trailing edge displacement thickness at each wing station is printed every time the boundary layer is recalculated along with the computed skin

friction coefficient. The boundary layer summary includes printout of the local Reynolds number used in the boundary layer calculation, the local Mach number, the displacement thickness, the momentum thickness, and the separation index. A printer plot of wing sections before and after application of the displacement thickness is also printed every NPRV iterations.

MASS STORAGE OUTPUT

When the IPLOT flag is set, the program will output data to mass storage for plotting or other post-processing. The majority of data written to mass storage will be stored on logical unit 9. However, additional data will be stored on other units for design or viscous analysis runs. The definitions of these data are discussed in the following sections. The order and format of the data can be obtained from a listing of subroutine PLTOUT.

Data Stored on Logical Unit 8

TITLE1 - Test case title and description from input

TITLE2 - Test case title and description from input

MACH - Freestream mach number

AOA - Wing angle of attack

CLW - Computed wing lift coefficient

CDW - Computed wing drag coefficient

CMW - Computed wing pitching moment coefficient

CLG - Wing circulation lift coefficient

SREF - Wing reference area

CROOT - Wing root chord length

SPAN - Wing semi-span length

AR - Wing aspect ratio

JTPM1 - Number of chordwise computational grid planes on the wing

IDUM - Dummy integer

J - Index of chordwise grid plane along semi-span

ETA - Spanwise distance of grid plane J from the root normalized by the semi-span.

XLEW - X coordinate of wing leading edge on grid plane J

XTEW - X coordinate of wing trailing edge on grid plane J

CORDW - Local wing chord at grid plane J

NXB - Number of chordwise grid points on wing at grid plane J

JTIP - Index of the first grid plane off of the wing

YTIP - Eta location of the wing tip

XLET - X coordinate of the wing tip leading edge

XTET - X coordinate of the wing tip trailing edge

CTIP - Wing tip chord

XIN - X/C location of computed data

CPL - Lower surface pressure coefficient

CPU - Upper surface pressure coefficient

CLS - Sectional lift coefficient at grid plane J

CDS - Sectional drag coefficient at grid plane J

CMS - Sectional moment coefficient at grid plane J

TWIST - Twist angle of airfoil section at grid plane J

ZOCU - Wing section upper surface ordinates at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.

ZOCL - Wing section lower surface ordinates at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.

DZXU - Wing section upper surface slopes at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.

DZXL - Wing section lower surface slopes at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.

INU - Number of chordwise points used to define initial airfoil section upper surface.

INL - Number of chordwise points used to define initial airfoil section lower surface.

ZUPI - Airfoil section upper surface ordinates interpolated from the original input airfoil sections. ZUPI will change if relofting is used in design runs.

ZLPI - Airfoil section lower surface ordinates interpolated from original input airfoil sections. ZLPI will change if relofting is used in design runs.

ITCNT - Total number of iterations on all grids used in solution.

NSPT - The number of supersonic points at a given iteration.

CLGT - The circulation lift at a given iteration.

RMAXT - The maximum residual at a given iteration.

CMAXT - The maximum correction at a given iteration.

ZINU - X/C location of input airfoil upper surface ordinates.

XINL - X/C location of input airfoil lower surface ordinates.

XINUS - Initial values of XINU saved when IDESN .NE. 0.

XINLS - Initial values of XINL saved when IDESN .NE. 0.

ZUPS - Initial values of ZUPI saved when IDESN .NE. 0.

ZLPS - Initial values of ZLPI saved when IDESN .NE. 0.

Data Stored on Logical Unit 9 when ISVSHP .NE. 0.

TITLE1 - Test case title and description from input

NJD - Total number of inverse design stations

ETA - Spanwise distance of grid plane J from the root normalized by the semi-span.

NXB - Number of chordwise grid points on wing at grid plane J

XIN - X/C location of computed data

Data Stored on Logical Unit 20 when IVISC .NE. 0.

TITLE1 - Test case title and description from input

JTPM1 - Number of chordwise computational grid planes on the wing

NXB - Number of chordwise grid points on wing at grid plane J

XIN - X/C location of computed data

DPUOLD - Upper surface boundary layer displacement thickness

DPLOLD - Lower surface boundary layer displacement thickness

RESTART DATA

Data to restart either an analysis or design case from a previous run is stored on units 7 and 14 by subroutine SAVSOL. At the end of each case, the computational grid, reduced potential and circulation are stored in unformatted form on logical unit 7. For inverse design cases, the relofted ordinates resulting from the design are stored on logical unit 14 whenever ISRLOR .NE. 0.

APPENDIX A
SAMPLE DATA SETS

The following sample data sets were used in the evaluation of the direct/inverse design method.

SAMPLE DATA SET NO. 1
ONERA M6 VISCOUS INVERSE AT J=12

M6 VISCOUS INVERSE AT ONE STATION (J=12) USEING MODIFIED CP'S
MACH=0.8395 AOA=3.06

ONERA M6 ORDINATES- 50X30X30

| | 4 | 69 | 69 | 0 | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.000323 | 0.000551 | 0.000866 | 0.001287 | 0.001836 | 0.002544 | 0.003443 | |
| 0.004570 | 0.005975 | 0.007711 | 0.009841 | 0.012448 | 0.015617 | 0.019461 | 0.024107 | |
| 0.029701 | 0.036426 | 0.044485 | 0.054125 | 0.065630 | 0.079337 | 0.095635 | 0.114980 | |
| 0.137896 | 0.164998 | 0.191933 | 0.218710 | 0.245331 | 0.271798 | 0.298111 | 0.324273 | |
| 0.350283 | 0.376145 | 0.401857 | 0.427422 | 0.452844 | 0.478120 | 0.503251 | 0.528243 | |
| 0.553094 | 0.577804 | 0.602376 | 0.626810 | 0.651109 | 0.675273 | 0.699303 | 0.723199 | |
| 0.746966 | 0.770600 | 0.794106 | 0.817483 | 0.840732 | 0.863856 | 0.886823 | 0.906191 | |
| 0.922534 | 0.936335 | 0.947995 | 0.957851 | 0.966186 | 0.973236 | 0.979202 | 0.984251 | |
| 0.988525 | 0.992144 | 0.995208 | 0.997803 | 1.000000 | | | | |
| 0.000000 | 0.000323 | 0.000551 | 0.000866 | 0.001287 | 0.001836 | 0.002544 | 0.003443 | |
| 0.004570 | 0.005975 | 0.007711 | 0.009841 | 0.012448 | 0.015617 | 0.019461 | 0.024107 | |
| 0.029701 | 0.036426 | 0.044485 | 0.054125 | 0.065630 | 0.079337 | 0.095635 | 0.114980 | |
| 0.137896 | 0.164998 | 0.191933 | 0.218710 | 0.245331 | 0.271798 | 0.298111 | 0.324273 | |
| 0.350283 | 0.376145 | 0.401857 | 0.427422 | 0.452844 | 0.478120 | 0.503251 | 0.528243 | |
| 0.553094 | 0.577804 | 0.602376 | 0.626810 | 0.651109 | 0.675273 | 0.699303 | 0.723199 | |
| 0.746966 | 0.770600 | 0.794106 | 0.817483 | 0.840732 | 0.863856 | 0.886823 | 0.906191 | |
| 0.922534 | 0.936335 | 0.947995 | 0.957851 | 0.966186 | 0.973236 | 0.979202 | 0.984251 | |
| 0.988525 | 0.992144 | 0.995208 | 0.997803 | 1.000000 | | | | |
| 0.000000 | 0.003138 | 0.004096 | 0.005134 | 0.006260 | 0.007478 | 0.008796 | 0.010216 | |
| 0.011742 | 0.013371 | 0.015095 | 0.016898 | 0.018754 | 0.020622 | 0.022455 | 0.024200 | |
| 0.025825 | 0.027332 | 0.028791 | 0.030328 | 0.032014 | 0.033837 | 0.035774 | 0.037792 | |
| 0.039852 | 0.041909 | 0.043621 | 0.045051 | 0.046236 | 0.047199 | 0.047949 | 0.048490 | |
| 0.048818 | 0.048930 | 0.048820 | 0.048483 | 0.047935 | 0.047166 | 0.046190 | 0.045021 | |
| 0.043674 | 0.042168 | 0.040524 | 0.038761 | 0.036899 | 0.034954 | 0.032940 | 0.030866 | |
| 0.028737 | 0.026550 | 0.024303 | 0.021984 | 0.019584 | 0.017091 | 0.014505 | 0.012239 | |
| 0.010273 | 0.008583 | 0.007142 | 0.005922 | 0.004891 | 0.004018 | 0.003280 | 0.002655 | |
| 0.002126 | 0.001678 | 0.001298 | 0.000977 | 0.000705 | | | | |
| 0.000000 | -0.003138 | -0.004096 | -0.005134 | -0.006260 | -0.007478 | -0.008796 | -0.010216 | |
| -0.011742 | -0.013371 | -0.015095 | -0.016898 | -0.018754 | -0.020622 | -0.022455 | -0.024200 | |
| -0.025825 | -0.027332 | -0.028791 | -0.030328 | -0.032014 | -0.033837 | -0.035774 | -0.037792 | |
| -0.039852 | -0.041909 | -0.043621 | -0.045051 | -0.046236 | -0.047199 | -0.047949 | -0.048490 | |
| -0.048818 | -0.048930 | -0.048820 | -0.048483 | -0.047935 | -0.047166 | -0.046190 | -0.045021 | |
| -0.043674 | -0.042168 | -0.040524 | -0.038761 | -0.036899 | -0.034954 | -0.032940 | -0.030866 | |
| -0.028737 | -0.026550 | -0.024303 | -0.021984 | -0.019584 | -0.017091 | -0.014505 | -0.012239 | |
| -0.010273 | -0.008583 | -0.007142 | -0.005922 | -0.004891 | -0.004018 | -0.003280 | -0.002655 | |
| -0.002126 | -0.001678 | -0.001298 | -0.000977 | -0.000705 | | | | |

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**** END OF SECTION DATA ****

ONERA M6 PLANFORM DESCRIPTION

0.0 0.0 805.9 1196.3 690.68413 1143.5999
752960.07 646.07 201.475

1

2

0.0 0.0 1196.3 690.68413
.57735027 .57735027

1

2

0.0 805.9 1196.3 1143.5999
.28297148 .28297148

0.0 0.0 .20000 0.0 .60000 0.0 .99999 0.0

COARSE SKEWED MESH

&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0,NTIPLE=1&END

&XGRID NXON=10,NXFWD=7,NXAFT=8,XFWD=-5.0,XAFT=8.0&END

&YGRID NYON=20,NYOFF=10,YMAX=1.3&END

&ZGRID NZ=8,ZP=3.655,&END

&SOLVIN MACH=0.8395,AOA=3.06,MAXIT=200,OMEGX=1.92,

OMEGY=1.92,OMEGZ=1.92,RCONV=.00001,

CON=1.0,NGSEQ=3,BXI=0.0,IPRINT=0,ICIRPF=100,

IPLOT=0,IPU=8,OMEGG=1.2,IKLUNK=1,IDESN=0&END

MEDIUM SKEWED MESH

&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0&END

&XGRID NXON=25,NXFWD=10,NXAFT=10,XFWD=-5.0,XAFT=8.0&END

&YGRID NYON=20,NYOFF=10,YMAX=1.3&END

&ZGRID NZ=16,ZMAX=5.0&END

&SOLVIN MAXIT=400,OMEGX=1.95,

OMEGY=1.95,RCONV=.0001,IPRINT=0,ICIRPF=400,IVISC=1,NITRL=100,

OMEGZ=1.95,CON=1.0,BXI=0.0,NDIF=0,IRLOFT=3,NITRF=10,

IPLOT=0,IPU=8,OMEGG=1.2,IKLUNK=1,IDESN=2,ILED=16,

ITED=35,NITDSN=50,ISVSHP=1,IINV=1&END

&VISCDT ITR=10,NVISC=50,NPRV=401,NJPRV=9,RN=25000000.,DELCOR=.844&END

ONERA M6 INVERSE WITH CP MODS

12 12 50

| | | | | | | |
|----------|-----------|-----------|-----------|----------|----------|----------|
| .010101 | .030303 | .050505 | .070707 | .090909 | .111111 | .131313 |
| .151515 | .171717 | .191919 | .212121 | .232323 | .252525 | .272727 |
| .292929 | .313131 | .333333 | .353535 | .373737 | .393939 | .414141 |
| .434343 | .454545 | .474747 | .494949 | .515152 | .535354 | .555556 |
| .575758 | .595960 | .616162 | .636364 | .656566 | .676768 | .696970 |
| .717172 | .737374 | .757576 | .777778 | .797980 | .818182 | .838384 |
| .858586 | .878788 | .898990 | .919192 | .939394 | .959596 | .979798 |
| 1.000000 | | | | | | |
| -.346519 | -1.127327 | -1.172505 | -1.109415 | -.985884 | -.830017 | -.676677 |
| -.569370 | -.524577 | -.521298 | -.535000 | -.535000 | -.535000 | -.535000 |
| -.535000 | -.535000 | -.535000 | -.535000 | -.535000 | -.535000 | -.535000 |
| -.535000 | -.535000 | -.535000 | -.525000 | -.515000 | -.465000 | -.395000 |
| -.310000 | -.210000 | -.160000 | -.149000 | -.139435 | -.126411 | -.112294 |
| -.097759 | -.083227 | -.068499 | -.053475 | -.037875 | -.020879 | -.001868 |

.020060 .045692 .075811 .111197 .152444 .200354 .260610
.347980

TRAILING EDGE THICKNESS TARGETS

1

0.01

FINE SKEWED MESH

```
&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0&END
&XGRID NXON=50,NXFWD=20,NXAFT=20,XFWD=-5.0,XAFT=8.0&END
&YGRID NYON=20,NYOFF=10,YMAX=1.3&END
&ZGRID NZ=30,ZMAX=5.0&END
&SOLVIN MAXIT=400,OMEGX=1.85,OMEGY=1.85,OMEGZ=1.85,
      RCONV=.001,IPRINT=1,ICIRPF=400,NITRL=100,NITRF=10,
      IPLOT=1,IPU=8,OMEGG=1.2,IKLUNK=1,IPRSHP=0,ISRLOR=1,
      NJSHP=1,BXI=0.0,CON=1.0,ILED=31,ITED=70,NITDSN=1,IVISC=1&END
&VISCDT ITR=10,NVISC=50,NPRV=400,NJPRV=9,RN=25000000.,DELCOR=.844&END
```

SAMPLE DATA SET NO. 2
C5 INVISCID DESIGN AT J=1-19

C5 INVISCID INVERSE TEST CASE DESIGN STATIONS J=1-19

MACH=0.775 AOA=2.0

C5 ORDINATES

| | 5 | 31 | 31 | 0 | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.002500 | 0.005000 | 0.007500 | 0.010000 | 0.020000 | 0.040000 | 0.060000 | |
| 0.080000 | 0.100000 | 0.120000 | 0.140000 | 0.160000 | 0.180000 | 0.200000 | 0.250000 | |
| 0.300000 | 0.350000 | 0.400000 | 0.450000 | 0.500000 | 0.550000 | 0.600000 | 0.650000 | |
| 0.700000 | 0.750000 | 0.800000 | 0.850000 | 0.900000 | 0.950000 | 1.000000 | | |
| 0.000000 | 0.002500 | 0.005000 | 0.007500 | 0.010000 | 0.020000 | 0.040000 | 0.060000 | |
| 0.080000 | 0.100000 | 0.120000 | 0.140000 | 0.160000 | 0.180000 | 0.200000 | 0.250000 | |
| 0.300000 | 0.350000 | 0.400000 | 0.450000 | 0.500000 | 0.550000 | 0.600000 | 0.650000 | |
| 0.700000 | 0.750000 | 0.800000 | 0.850000 | 0.900000 | 0.950000 | 1.000000 | | |
| 0.005629 | 0.011618 | 0.014906 | 0.017438 | 0.019562 | 0.025964 | 0.033540 | 0.039428 | |
| 0.043911 | 0.047641 | 0.050505 | 0.053343 | 0.055845 | 0.057955 | 0.060064 | 0.063924 | |
| 0.066743 | 0.068500 | 0.069185 | 0.069162 | 0.067669 | 0.065596 | 0.062679 | 0.059085 | |
| 0.054549 | 0.049070 | 0.042514 | 0.034879 | 0.025692 | 0.014690 | 0.001289 | | |
| 0.005629 | -0.004190 | -0.007038 | -0.008982 | -0.010615 | -0.015610 | -0.023116 | -0.029223 | |
| -0.034191 | -0.038352 | -0.041568 | -0.044785 | -0.047620 | -0.050058 | -0.052488 | -0.056812 | |
| -0.059852 | -0.061615 | -0.062032 | -0.061170 | -0.059031 | -0.055746 | -0.051383 | -0.045872 | |
| -0.039654 | -0.032971 | -0.025789 | -0.018461 | -0.011621 | -0.005749 | -0.001289 | | |

| T | F | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.005809 | 0.011672 | 0.014924 | 0.017571 | 0.019632 | 0.026053 | 0.033823 | 0.039802 | |
| 0.044405 | 0.048000 | 0.051196 | 0.054105 | 0.056622 | 0.058782 | 0.060932 | 0.064926 | |
| 0.067822 | 0.069720 | 0.070620 | 0.070620 | 0.069721 | 0.067824 | 0.065028 | 0.061433 | |
| 0.056841 | 0.051152 | 0.044167 | 0.035851 | 0.025811 | 0.014433 | 0.001102 | | |
| 0.005809 | -0.003927 | -0.007067 | -0.009012 | -0.010608 | -0.015152 | -0.021136 | -0.025732 | |
| -0.029260 | -0.032049 | -0.034070 | -0.036030 | -0.037737 | -0.039097 | -0.040457 | -0.042838 | |
| -0.044252 | -0.044963 | -0.044878 | -0.044076 | -0.042477 | -0.040179 | -0.037182 | -0.033486 | |
| -0.029001 | -0.024299 | -0.019404 | -0.014604 | -0.009811 | -0.005317 | -0.001102 | | |

| T | F | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.005803 | 0.011569 | 0.014967 | 0.017536 | 0.019638 | 0.026077 | 0.033879 | 0.039897 | |
| 0.044300 | 0.047900 | 0.051409 | 0.054366 | 0.056903 | 0.059081 | 0.061220 | 0.065323 | |
| 0.06824- | 0.070083 | 0.071061 | 0.071169 | 0.070280 | 0.068432 | 0.065714 | 0.062026 | |
| 0.057580 | 0.051847 | 0.044714 | 0.035995 | 0.025915 | 0.013754 | 0.001094 | | |
| 0.005803 | -0.003995 | -0.007043 | -0.008954 | -0.010571 | -0.014972 | -0.020606 | -0.024799 | |
| -0.027976 | -0.030345 | -0.032038 | -0.033668 | -0.035028 | -0.036028 | -0.037028 | -0.038832 | |
| -0.039827 | -0.040179 | -0.039969 | -0.039203 | -0.037795 | -0.035693 | -0.033193 | -0.029862 | |
| -0.026058 | -0.021945 | -0.017726 | -0.013595 | -0.009463 | -0.005225 | -0.001094 | | |

| T | F | | | | | | | |
|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.006032 | 0.012488 | 0.015727 | 0.018285 | 0.020444 | 0.026978 | 0.034727 | 0.040687 | |
| 0.045100 | 0.048900 | 0.052100 | 0.055103 | 0.057433 | 0.059633 | 0.061791 | 0.065792 | |
| 0.068588 | 0.070417 | 0.071149 | 0.071025 | 0.069806 | 0.067614 | 0.064577 | 0.060598 | |
| 0.055848 | 0.050013 | 0.042853 | 0.034400 | 0.024790 | 0.013589 | 0.001108 | | |
| 0.006032 | -0.003871 | -0.007209 | -0.009141 | -0.010737 | -0.015212 | -0.020623 | -0.024567 | |

-0.027415 -0.029582 -0.031085 -0.032517 -0.033762 -0.034738 -0.035713 -0.037375
 -0.038636 -0.039376 -0.039394 -0.038.90 -0.037429 -0.035359 -0.032617 -0.029446
 -0.025451 -0.021305 -0.017055 -0.012808 -0.008666 -0.004766 -0.001108

| T | F | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000745 | 0.015880 | 0.019650 | 0.022717 | 0.024966 | 0.031731 | 0.039420 | 0.045103 | |
| 0.049100 | 0.052765 | 0.055845 | 0.058205 | 0.060562 | 0.062634 | 0.064687 | 0.068398 | |
| 0.071018 | 0.071863 | 0.071501 | 0.069947 | 0.067091 | 0.063104 | 0.058319 | 0.052545 | |
| 0.045971 | 0.038907 | 0.031906 | 0.024620 | 0.017412 | 0.009606 | 0.001006 | | |
| 0.000745 | -0.002368 | -0.006812 | -0.009262 | -0.011326 | -0.016277 | -0.020702 | -0.023207 | |
| -0.024618 | -0.025424 | -0.025906 | -0.026314 | -0.026715 | -0.027243 | -0.027735 | -0.029567 | |
| -0.032057 | -0.034703 | -0.036336 | -0.036447 | -0.035379 | -0.033157 | -0.029948 | -0.026146 | |
| -0.021978 | -0.017757 | -0.012968 | -0.008576 | -0.004595 | -0.002006 | -0.001006 | | |

*** END OF C5 AIRFOIL DATA ***

C5 PLANFORM DESCRIPTION

0.0 0.0 79.21 178.80 94.36 123.36

18720.0 221.36 55.34

2

2

0.0 0.0 82.0 44.14

.538292683.538292683

2

82.0 44.14 178.80 94.36

.518801653.518801653

2

2

0.0 79.21 82.0 93.21

.170731707.170731707

2

82.0 93.21 178.80 123.36

.311466942.311466942

0.0 4.18 .388702461 2.9 .458612975 2.68 .604026846 2.18

1.0 -0.9

26X30X8 MESH

&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0,NTIPLE=1&END

&XGRID NXON=10,NXFWD=8,NXAFT=8,XFWD=-5.0,XAFT=8.0&END

&YGRID NYON=20,NYOFF=10,YMAX=1.5&END

&ZGRID NZ=8,ZP=3.3&END

&SOLVIN MACH=.775,AOA=2.00,MAXIT=220,OMEGX=1.92,

OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=220,

OMEGZ=1.92,CON=1.0,NGSEQ=3,BXI=0.0,

IPLT=0,IPU=8,OMEGG=1.2,IKLUNK=0,IDESN=0&END

45X30X16 MESH

&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0,NTIPLE=1&END

&XGRID NXON=25,NXFWD=10,NXAFT=10,XFWD=-5.0,XAFT=8.0&END

&YGRID NYON=20,NYOFF=10,YMAX=1.5&END

&ZGRID NZ=16,ZP=1.75,ZMAX=5.0&END

&SOLVIN MAXIT=300,OMEGX=1.92,

OMEGY=1.92,RCONV=.0001,IPRINT=0,ICIRPF=300,NITRL=100,NJSHP=4,

OMEGZ=1.92,CON=1.0,IPRSHP=0,IRLOFT=3,

I PLOT=0, IPU=8, OMEGG=1.2, IKLUNK=0, IDESN=2, ILED=16, NITRF=10,
ITED=35, NITDSN=50, ISVSHP=1, IINV=1, IVISC=0&END

C5 INV MOD 4 LINEAR CP RECOVERY J=1-19

| 1 | 19 | 50 | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.010101 | 0.030303 | 0.050505 | 0.070707 | 0.090909 | 0.111111 | 0.131313 | |
| 0.151515 | 0.171717 | 0.191919 | 0.212121 | 0.232323 | 0.252525 | 0.272727 | |
| 0.292929 | 0.313131 | 0.333333 | 0.353535 | 0.373737 | 0.393939 | 0.414141 | |
| 0.434343 | 0.454545 | 0.474747 | 0.494949 | 0.515152 | 0.535354 | 0.555556 | |
| 0.575758 | 0.595960 | 0.616162 | 0.636364 | 0.656566 | 0.676768 | 0.696970 | |
| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 | |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 | |
| 1.000000 | | | | | | | |
| 0.250413 | -0.547996 | -0.690000 | -0.750000 | -0.770000 | -0.790000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.790000 | |
| -0.780000 | -0.760000 | -0.720000 | -0.680000 | -0.620000 | -0.560000 | -0.480000 | |
| -0.440000 | -0.350000 | -0.260000 | -0.160000 | -0.040000 | 0.065930 | 0.179936 | |
| 0.345951 | | | | | | | |
| 0.010101 | 0.030303 | 0.050505 | 0.070707 | 0.090909 | 0.111111 | 0.131313 | |
| 0.151515 | 0.171717 | 0.191919 | 0.212121 | 0.232323 | 0.252525 | 0.272727 | |
| 0.292929 | 0.313131 | 0.333333 | 0.353535 | 0.373737 | 0.393939 | 0.414141 | |
| 0.434343 | 0.454545 | 0.474747 | 0.494949 | 0.515152 | 0.535354 | 0.555556 | |
| 0.575758 | 0.595960 | 0.616162 | 0.636364 | 0.656566 | 0.676768 | 0.696970 | |
| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 | |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 | |
| 1.000000 | | | | | | | |
| -0.133011 | -0.834330 | -0.865831 | -0.850000 | -0.830000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | |
| -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.800000 | -0.790000 | -0.770000 | |
| -0.740000 | -0.700000 | -0.670000 | -0.610000 | -0.550000 | -0.500000 | -0.420000 | |
| -0.350000 | -0.250000 | -0.160000 | -0.090000 | 0.020967 | 0.103324 | 0.210316 | |
| 0.358176 | | | | | | | |
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| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 |
| 1.000000 | | | | | | |
| -0.789175 | -1.184176 | -1.268442 | -1.315068 | -1.351130 | -1.346501 | -1.335827 |
| -1.312219 | -1.276365 | -1.245651 | -1.220000 | -1.210000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.170000 | -1.110000 |
| -1.040000 | -0.974283 | -0.908566 | -0.842848 | -0.777131 | -0.711414 | -0.645697 |
| -0.579979 | -0.514262 | -0.448545 | -0.382828 | -0.317111 | -0.251394 | -0.185677 |
| -0.119959 | -0.054242 | 0.011475 | 0.077192 | 0.142909 | 0.208627 | 0.274344 |
| 0.340061 | | | | | | |
| 0.010101 | 0.030303 | 0.050505 | 0.070707 | 0.090909 | 0.111111 | 0.131313 |

| | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 0.151515 | 0.171717 | 0.191919 | 0.212121 | 0.232323 | 0.252525 | 0.272727 |
| 0.292929 | 0.313131 | 0.333333 | 0.353535 | 0.373737 | 0.393939 | 0.414141 |
| 0.434343 | 0.454545 | 0.474747 | 0.494949 | 0.515152 | 0.535354 | 0.555556 |
| 0.575758 | 0.595960 | 0.616162 | 0.636364 | 0.656566 | 0.676768 | 0.696970 |
| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 |
| 1.000000 | | | | | | |
| -0.789175 | -1.184176 | -1.268442 | -1.315068 | -1.351130 | -1.346501 | -1.335827 |
| -1.312219 | -1.276365 | -1.245651 | -1.220000 | -1.210000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.170000 | -1.110000 |
| -1.040000 | -0.974283 | -0.908566 | -0.842848 | -0.777131 | -0.711414 | -0.645697 |
| -0.579979 | -0.514262 | -0.448545 | -0.382828 | -0.317111 | -0.251394 | -0.185677 |
| -0.119959 | -0.054242 | 0.011475 | 0.077192 | 0.142909 | 0.208627 | 0.274344 |
| 0.340061 | | | | | | |
| 0.010101 | 0.030303 | 0.050505 | 0.070707 | 0.090909 | 0.111111 | 0.131313 |
| 0.151515 | 0.171717 | 0.191919 | 0.212121 | 0.232323 | 0.252525 | 0.272727 |
| 0.292929 | 0.313131 | 0.333333 | 0.353535 | 0.373737 | 0.393939 | 0.414141 |
| 0.434343 | 0.454545 | 0.474747 | 0.494949 | 0.515152 | 0.535354 | 0.555556 |
| 0.575758 | 0.595960 | 0.616162 | 0.636364 | 0.656566 | 0.676768 | 0.696970 |
| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 |
| 1.000000 | | | | | | |
| -0.789175 | -1.184176 | -1.268442 | -1.315068 | -1.351130 | -1.346501 | -1.335827 |
| -1.312219 | -1.276365 | -1.245651 | -1.220000 | -1.210000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.170000 | -1.110000 |
| -1.040000 | -0.974283 | -0.908566 | -0.842848 | -0.777131 | -0.711414 | -0.645697 |
| -0.579979 | -0.514262 | -0.448545 | -0.382828 | -0.317111 | -0.251394 | -0.185677 |
| -0.119959 | -0.054242 | 0.011475 | 0.077192 | 0.142909 | 0.208627 | 0.274344 |
| 0.340061 | | | | | | |
| 0.010101 | 0.030303 | 0.050505 | 0.070707 | 0.090909 | 0.111111 | 0.131313 |
| 0.151515 | 0.171717 | 0.191919 | 0.212121 | 0.232323 | 0.252525 | 0.272727 |
| 0.292929 | 0.313131 | 0.333333 | 0.353535 | 0.373737 | 0.393939 | 0.414141 |
| 0.434343 | 0.454545 | 0.474747 | 0.494949 | 0.515152 | 0.535354 | 0.555556 |
| 0.575758 | 0.595960 | 0.616162 | 0.636364 | 0.656566 | 0.676768 | 0.696970 |
| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 |
| 1.000000 | | | | | | |
| -0.789175 | -1.184176 | -1.268442 | -1.315068 | -1.351130 | -1.346501 | -1.335827 |
| -1.312219 | -1.276365 | -1.245651 | -1.220000 | -1.210000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.170000 | -1.110000 |
| -1.040000 | -0.974283 | -0.908566 | -0.842848 | -0.777131 | -0.711414 | -0.645697 |
| -0.579979 | -0.514262 | -0.448545 | -0.382828 | -0.317111 | -0.251394 | -0.185677 |
| -0.119959 | -0.054242 | 0.011475 | 0.077192 | 0.142909 | 0.208627 | 0.274344 |
| 0.340061 | | | | | | |
| 0.010101 | 0.030303 | 0.050505 | 0.070707 | 0.090909 | 0.111111 | 0.131313 |
| 0.151515 | 0.171717 | 0.191919 | 0.212121 | 0.232323 | 0.252525 | 0.272727 |

| | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 0.292929 | 0.313131 | 0.333333 | 0.353535 | 0.373737 | 0.393939 | 0.414141 |
| 0.434343 | 0.454545 | 0.474747 | 0.494949 | 0.515152 | 0.535354 | 0.555556 |
| 0.575758 | 0.595960 | 0.616162 | 0.636364 | 0.656566 | 0.676768 | 0.696970 |
| 0.717172 | 0.737374 | 0.757576 | 0.777778 | 0.797980 | 0.818182 | 0.838384 |
| 0.858586 | 0.878788 | 0.898990 | 0.919192 | 0.939394 | 0.959596 | 0.979798 |
| 1.000000 | | | | | | |
| -0.789175 | -1.184176 | -1.268442 | -1.315068 | -1.351130 | -1.346501 | -1.335827 |
| -1.312219 | -1.276365 | -1.245651 | -1.220000 | -1.210000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 |
| -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.200000 | -1.170000 | -1.110000 |
| -1.040000 | -0.974283 | -0.908566 | -0.842848 | -0.777131 | -0.711414 | -0.645697 |
| -0.579979 | -0.514262 | -0.448545 | -0.382828 | -0.317111 | -0.251394 | -0.185677 |
| -0.119959 | -0.054242 | 0.011475 | 0.077192 | 0.142909 | 0.208627 | 0.274344 |

0.340061

TRAILING EDGE THICKNESS TARGETS

19

| | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|
| 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 |
| 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | | |

90X30X30 GRID

```

&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0&END
&XGRID NXON=50,NXFWD=20,NXAFT=20&END
&YGRID NYON=20,NYOFF=10,YMAX=1.5&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=300,OMEGX=1.90,NITRL=20,NITRF=40,
      OMEGY=1.90,RCONV=.001,IPRINT=1,ICIRPF=300,ISVSHP=1,
      OMEGZ=1.90,IPLOT=1,IPU=8,OMEGG=1.2,IKLUNK=0,ISRLOR=1,
      BXI=0.0,CON=1.0,ILED=31,ITED=70,NITDSN=1,IPRSHP=0&END

```

SAMPLE DATA SET NO. 3
 RAE WING BODY TEST CASE

RAE WING A WING BODY TEST CASE

MACH=0.80 AOA=2.0

RAE WING "A" ORDINATES

| 2 | 86 | 86 | 0 | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.001000 | 0.002000 | 0.003000 | 0.004000 | 0.005000 | 0.006000 | 0.007000 | |
| 0.007500 | 0.008000 | 0.009000 | 0.010000 | 0.012000 | 0.012500 | 0.014000 | 0.016000 | |
| 0.018000 | 0.020000 | 0.025000 | 0.030000 | 0.035000 | 0.040000 | 0.050000 | 0.060000 | |
| 0.070000 | 0.075000 | 0.080000 | 0.090000 | 0.100000 | 0.120000 | 0.140000 | 0.150000 | |
| 0.160000 | 0.180000 | 0.200000 | 0.220000 | 0.240000 | 0.250000 | 0.260000 | 0.280000 | |
| 0.300000 | 0.320000 | 0.340000 | 0.350000 | 0.360000 | 0.380000 | 0.400000 | 0.420000 | |
| 0.440000 | 0.450000 | 0.460000 | 0.480000 | 0.500000 | 0.520000 | 0.540000 | 0.550000 | |
| 0.560000 | 0.580000 | 0.600000 | 0.620000 | 0.640000 | 0.650000 | 0.660000 | 0.680000 | |
| 0.700000 | 0.720000 | 0.740000 | 0.750000 | 0.760000 | 0.780000 | 0.800000 | 0.820000 | |
| 0.840000 | 0.850000 | 0.860000 | 0.880000 | 0.900000 | 0.920000 | 0.925000 | 0.940000 | |
| 0.950000 | 0.960000 | 0.975000 | 0.980000 | 0.987500 | 1.000000 | | | |
| 0.000000 | 0.001000 | 0.002000 | 0.003000 | 0.004000 | 0.005000 | 0.006000 | 0.007000 | |
| 0.007500 | 0.008000 | 0.009000 | 0.010000 | 0.012000 | 0.012500 | 0.014000 | 0.016000 | |
| 0.018000 | 0.020000 | 0.025000 | 0.030000 | 0.035000 | 0.040000 | 0.050000 | 0.060000 | |
| 0.070000 | 0.075000 | 0.080000 | 0.090000 | 0.100000 | 0.120000 | 0.140000 | 0.150000 | |
| 0.160000 | 0.180000 | 0.200000 | 0.220000 | 0.240000 | 0.250000 | 0.260000 | 0.280000 | |
| 0.300000 | 0.320000 | 0.340000 | 0.350000 | 0.360000 | 0.380000 | 0.400000 | 0.420000 | |
| 0.440000 | 0.450000 | 0.460000 | 0.480000 | 0.500000 | 0.520000 | 0.540000 | 0.550000 | |
| 0.560000 | 0.580000 | 0.600000 | 0.620000 | 0.640000 | 0.650000 | 0.660000 | 0.680000 | |
| 0.700000 | 0.720000 | 0.740000 | 0.750000 | 0.760000 | 0.780000 | 0.800000 | 0.820000 | |
| 0.840000 | 0.850000 | 0.860000 | 0.880000 | 0.900000 | 0.920000 | 0.925000 | 0.940000 | |
| 0.950000 | 0.960000 | 0.975000 | 0.980000 | 0.987500 | 1.000000 | | | |
| 0.000000 | 0.003515 | 0.004966 | 0.006078 | 0.007013 | 0.007835 | 0.008576 | 0.009256 | |
| 0.009578 | 0.009888 | 0.010480 | 0.011039 | 0.012074 | 0.012318 | 0.013022 | 0.013901 | |
| 0.014721 | 0.015494 | 0.017257 | 0.018832 | 0.020262 | 0.021577 | 0.023903 | 0.026008 | |
| 0.027863 | 0.028722 | 0.029540 | 0.031067 | 0.032466 | 0.034938 | 0.037046 | 0.037982 | |
| 0.038847 | 0.040380 | 0.041674 | 0.042746 | 0.043610 | 0.043966 | 0.044271 | 0.044730 | |
| 0.044972 | 0.044960 | 0.044752 | 0.044582 | 0.044376 | 0.043855 | 0.043205 | 0.042438 | |
| 0.041565 | 0.041091 | 0.040595 | 0.039539 | 0.038403 | 0.037196 | 0.035924 | 0.035265 | |
| 0.034592 | 0.033209 | 0.031779 | 0.030308 | 0.028803 | 0.028039 | 0.027267 | 0.025707 | |
| 0.024126 | 0.022531 | 0.020926 | 0.020121 | 0.019317 | 0.017707 | 0.016097 | 0.014487 | |
| 0.012878 | 0.012073 | 0.011268 | 0.009658 | 0.008049 | 0.006439 | 0.006036 | 0.004829 | |
| 0.004024 | 0.003219 | 0.002012 | 0.001610 | 0.001006 | 0.000000 | | | |
| 0.000000 | -0.003515 | -0.004966 | -0.006078 | -0.007013 | -0.007835 | -0.008576 | -0.009256 | |
| -0.009578 | -0.009888 | -0.010480 | -0.011039 | -0.012074 | -0.012318 | -0.013022 | -0.013901 | |
| -0.014721 | -0.015494 | -0.017257 | -0.018832 | -0.020262 | -0.021577 | -0.023903 | -0.026008 | |
| -0.027863 | -0.028722 | -0.029540 | -0.031067 | -0.032466 | -0.034938 | -0.037046 | -0.037982 | |
| -0.038847 | -0.040380 | -0.041674 | -0.042746 | -0.043610 | -0.043966 | -0.044271 | -0.044730 | |
| -0.044972 | -0.044960 | -0.044752 | -0.044582 | -0.044376 | -0.043855 | -0.043205 | -0.042438 | |

-0.041565 -0.041091 -0.040595 -0.039539 -0.038403 -0.037196 -0.035924 -0.035265
 -0.034592 -0.033209 -0.031779 -0.030308 -0.028803 -0.028039 -0.027267 -0.025707
 -0.024126 -0.022531 -0.020926 -0.020121 -0.019317 -0.017707 -0.016097 -0.014487
 -0.012878 -0.012073 -0.011268 -0.009658 -0.008049 -0.006439 -0.006036 -0.004829
 -0.004024 -0.003219 -0.002012 -0.001610 -0.001006 0.000000

T T

*** END OF RAE AIRFOIL DATA ***

RAE WING PLANFORM DESCRIPTION

| | | | | | |
|------|-----|-----|-------|-----------|-----------|
| 0.0 | 0.0 | 8.0 | 15.0 | 11.160306 | 14.160306 |
| 82.5 | | 5.5 | 7.208 | | |

1

2

| | | | |
|-----|-----|------|-----------|
| 0.0 | 0.0 | 15.0 | 11.160306 |
|-----|-----|------|-----------|

| | | | |
|---------|--|---------|--|
| .744020 | | .744020 | |
|---------|--|---------|--|

1

2

| | | | |
|-----|-----|------|-----------|
| 0.0 | 8.0 | 15.0 | 14.160306 |
|-----|-----|------|-----------|

| | | | |
|---------|--|---------|--|
| .410946 | | .410946 | |
|---------|--|---------|--|

| | | | |
|-----|-----|-----|-----|
| 0.0 | 0.0 | 1.0 | 0.0 |
|-----|-----|-----|-----|

26X30X8

&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0,NTIPLE=1&END

&XGRID NXON=10,NXFWD=8,NXAFT=8.XFWD=-5.XAFT=8.0&END

&YGRID NYON=20.NYOFF=10,YMAX=1.4&END

&ZGRID NZ=8,ZP=3.3&END

&SOLVIN MACH=0.80,AOA=2.0,MAXIT=400.OMEGX=1.92,

OMEGY=1.92,RCONV=.00001.IPRINT=0,ICIRPF=100,

OMEGZ=1.92.CON=1.0,NGSEQ=3,BXI=0.0.NF=30,

IPLOT=0,IPU=8.OMEGG=1.2,IKLUNK=1,IFUSE=2&END

| XBODY | YBODY | ZBODY | RBODY | LENGTH | ALF |
|--------|-------|-------|-------|--------|-----|
| 22.232 | 3. | 0. | 3.0 | 70. | 16. |

NST

20

XF AREA

| | |
|-----|-----|
| 0.0 | 0.0 |
|-----|-----|

| | |
|-----|---------|
| 2.0 | 2.58155 |
|-----|---------|

| | |
|-----|---------|
| 4.0 | 8.33570 |
|-----|---------|

| | |
|-----|----------|
| 6.0 | 14.87571 |
|-----|----------|

| | |
|-----|----------|
| 8.0 | 20.62897 |
|-----|----------|

| | |
|------|----------|
| 10.0 | 24.78582 |
|------|----------|

| | |
|------|----------|
| 12.0 | 27.18065 |
|------|----------|

| | |
|------|----------|
| 14.0 | 28.13185 |
|------|----------|

| | |
|------|----------|
| 16.0 | 28.27433 |
|------|----------|

| | |
|------|----------|
| 22.0 | 28.27433 |
|------|----------|

| | |
|------|----------|
| 28.0 | 28.27433 |
|------|----------|

| | |
|------|----------|
| 32.0 | 28.27433 |
|------|----------|

| | |
|------|----------|
| 36.0 | 28.27433 |
|------|----------|

| | |
|------|----------|
| 40.0 | 28.27433 |
|------|----------|

| | |
|-------|----------|
| 45.95 | 28.27433 |
|-------|----------|

| | |
|------|----------|
| 47.0 | 21.64754 |
|------|----------|

48.0 15.90431
49.0 11.04466
50.0 7.06858
70. 3.14159

45X30X16 GRID

&GPARM IPRNTG=0,WBCPRT=.F.&END
&XGRID NXON=25,NXFWD=10,NXAFT=10&END
&YGRID NYON=20,NYOFF=10,YMAX=1.4,RTSWCH=1.0&END
&ZGRID NZ=16,ZMAX=5.0&END
&SOLVIN MAXIT=400,OMEGX=1.9,
 OMEGY=1.9,RCONV=.0001,ICIRPF=100,
 OMEGZ=1.9&END

90X30X30 GRID

&GPARM IPRNTG=0&END
&XGRID NXON=50,NXFWD=20,NXAFT=20&END
&YGRID NYON=20.NYOFF=10,YMAX=1.4&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=100,OMEGX=1.9,
 OMEGY=1.9,RCONV=.001,IPRINT=1,ICIRPF=50,
 OMEGZ=1.9,IPLOT=1,IPU=8,OMEGG=1.2,IKLUNK=1&END

SAMPLE DATA SET NO. 4
F14 INVISCID ANALYSIS

F14 INVISCID ANALYSIS WITH BOPPE CODE ORDINATES 2 GRIDS

MACH = .8 AOA=1.4

F14 ORDINATES-FROM GRUMMAN REPORT

| | 9 | 50 | 50 | 0 | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.001910 | 0.004960 | 0.009950 | 0.020000 | 0.039930 | 0.060000 | 0.080000 | |
| 0.100000 | 0.120000 | 0.140000 | 0.160000 | 0.180000 | 0.200000 | 0.220000 | 0.240000 | |
| 0.260000 | 0.280000 | 0.300000 | 0.320000 | 0.340000 | 0.360000 | 0.380000 | 0.400000 | |
| 0.420000 | 0.440000 | 0.460000 | 0.480000 | 0.500000 | 0.520000 | 0.560000 | 0.600000 | |
| 0.640000 | 0.680000 | 0.700000 | 0.720000 | 0.740000 | 0.760000 | 0.780000 | 0.800000 | |
| 0.820000 | 0.840000 | 0.860000 | 0.880000 | 0.900000 | 0.920000 | 0.940000 | 0.960000 | |
| 0.980000 | 1.000000 | | | | | | | |
| 0.000000 | 0.001910 | 0.004960 | 0.009950 | 0.020000 | 0.039930 | 0.060000 | 0.080000 | |
| 0.100000 | 0.120000 | 0.140000 | 0.160000 | 0.180000 | 0.200000 | 0.220000 | 0.240000 | |
| 0.260000 | 0.280000 | 0.300000 | 0.320000 | 0.340000 | 0.360000 | 0.380000 | 0.400000 | |
| 0.420000 | 0.440000 | 0.460000 | 0.480000 | 0.500000 | 0.520000 | 0.560000 | 0.600000 | |
| 0.640000 | 0.680000 | 0.700000 | 0.720000 | 0.740000 | 0.760000 | 0.780000 | 0.800000 | |
| 0.820000 | 0.840000 | 0.860000 | 0.880000 | 0.900000 | 0.920000 | 0.940000 | 0.960000 | |
| 0.980000 | 1.000000 | | | | | | | |
| 0.004660 | 0.010460 | 0.014220 | 0.018540 | 0.025040 | 0.034540 | 0.041700 | 0.047300 | |
| 0.051770 | 0.055340 | 0.058180 | 0.060420 | 0.062140 | 0.063440 | 0.064370 | 0.064990 | |
| 0.065330 | 0.065430 | 0.065320 | 0.065020 | 0.064560 | 0.063950 | 0.063200 | 0.062320 | |
| 0.061330 | 0.060230 | 0.059030 | 0.057730 | 0.056350 | 0.054870 | 0.051650 | 0.048100 | |
| 0.044240 | 0.040070 | 0.037880 | 0.035610 | 0.033280 | 0.030880 | 0.028420 | 0.025900 | |
| 0.023320 | 0.020690 | 0.018000 | 0.015280 | 0.012510 | 0.009710 | 0.006880 | 0.004030 | |
| 0.001170 | -0.001710 | | | | | | | |
| 0.004660 | -0.001580 | -0.005400 | -0.009910 | -0.015700 | -0.022670 | -0.027140 | -0.030320 | |
| -0.032720 | -0.034590 | -0.036060 | -0.037210 | -0.038100 | -0.038760 | -0.039210 | -0.039490 | |
| -0.039600 | -0.039570 | -0.039400 | -0.039120 | -0.038730 | -0.038240 | -0.037660 | -0.037010 | |
| -0.036290 | -0.035510 | -0.034680 | -0.033810 | -0.032900 | -0.031960 | -0.030000 | -0.027960 | |
| -0.025870 | -0.023770 | -0.022720 | -0.021660 | -0.020620 | -0.019570 | -0.018540 | -0.017510 | |
| -0.016490 | -0.015470 | -0.014470 | -0.013470 | -0.012480 | -0.011500 | -0.010520 | -0.009550 | |
| -0.008580 | -0.007610 | | | | | | | |

| T | F | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.007560 | 0.013570 | 0.017100 | 0.021010 | 0.026720 | 0.034850 | 0.040950 | 0.045820 | |
| 0.049830 | 0.053170 | 0.055960 | 0.058270 | 0.060170 | 0.061700 | 0.062910 | 0.063810 | |
| 0.064440 | 0.064820 | 0.064960 | 0.064890 | 0.064620 | 0.064160 | 0.063520 | 0.062710 | |
| 0.061750 | 0.060640 | 0.059380 | 0.058000 | 0.056480 | 0.054850 | 0.051240 | 0.047220 | |
| 0.042840 | 0.038120 | 0.035660 | 0.033130 | 0.030540 | 0.027900 | 0.025210 | 0.022470 | |
| 0.019700 | 0.016890 | 0.014050 | 0.011190 | 0.008300 | 0.005400 | 0.002490 | -0.000430 | |
| -0.003350 | -0.006280 | | | | | | | |
| 0.007560 | 0.001820 | -0.001760 | -0.005480 | -0.010130 | -0.015670 | -0.019220 | -0.021780 | |
| -0.023750 | -0.025320 | -0.026610 | -0.027680 | -0.028570 | -0.029320 | -0.029940 | -0.030460 | |
| -0.030870 | -0.031200 | -0.031440 | -0.031600 | -0.031680 | -0.031690 | -0.031630 | -0.031500 | |

-0.031300 -0.031050 -0.030730 -0.030360 -0.029930 -0.029450 -0.028340 -0.027060
 -0.025620 -0.024050 -0.023220 -0.022360 -0.021480 -0.020580 -0.019660 -0.018720
 -0.017770 -0.016800 -0.015820 -0.014840 -0.013850 -0.012850 -0.011850 -0.010850
 -0.009840 -0.008840

| T | F |
|-----------|-----------|
| 0.008780 | 0.014880 |
| 0.049010 | 0.052260 |
| 0.064060 | 0.064560 |
| 0.061930 | 0.060810 |
| 0.042240 | 0.037300 |
| 0.018180 | 0.015290 |
| -0.005260 | -0.008210 |
| 0.008780 | 0.003240 |
| -0.019970 | -0.021420 |
| -0.027200 | -0.027670 |
| -0.029200 | -0.029170 |
| -0.025520 | -0.024170 |
| -0.018310 | -0.017360 |
| -0.010370 | -0.009350 |

| T | F |
|-----------|-----------|
| 0.007220 | 0.013270 |
| 0.046820 | 0.050100 |
| 0.062910 | 0.063590 |
| 0.062050 | 0.061050 |
| 0.043170 | 0.038280 |
| 0.019270 | 0.016400 |
| -0.004000 | -0.006920 |
| 0.007220 | 0.001650 |
| -0.020290 | -0.021640 |
| -0.027230 | -0.027720 |
| -0.029450 | -0.029440 |
| -0.025700 | -0.024240 |
| -0.017720 | -0.016650 |
| -0.008690 | -0.007530 |

| T | F |
|-----------|-----------|
| 0.003160 | 0.009280 |
| 0.043410 | 0.046820 |
| 0.060980 | 0.061890 |
| 0.062070 | 0.061310 |
| 0.045450 | 0.040870 |
| 0.022700 | 0.019920 |
| 0.000040 | -0.002820 |
| 0.003160 | -0.002590 |
| -0.023750 | -0.025010 |
| -0.030100 | -0.030520 |
| -0.031580 | -0.031440 |
| -0.026050 | -0.024180 |
| -0.016060 | -0.014740 |
| -0.004940 | -0.003500 |

| T | F | | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|--|
| -0.002100 | 0.004120 | 0.007540 | 0.011340 | 0.016800 | 0.024410 | 0.030160 | 0.034880 | | |
| 0.038930 | 0.042490 | 0.045650 | 0.048450 | 0.050940 | 0.053140 | 0.055070 | 0.056750 | | |
| 0.058170 | 0.059360 | 0.060320 | 0.061060 | 0.061580 | 0.061890 | 0.062000 | 0.061910 | | |
| 0.061640 | 0.061180 | 0.060540 | 0.059740 | 0.058770 | 0.057650 | 0.054960 | 0.051730 | | |
| 0.048020 | 0.043880 | 0.041680 | 0.039390 | 0.037020 | 0.034580 | 0.032090 | 0.029540 | | |
| 0.026940 | 0.024310 | 0.021640 | 0.018940 | 0.016230 | 0.013490 | 0.010750 | 0.008000 | | |
| 0.005250 | 0.002490 | | | | | | | | |
| -0.002100 | -0.007870 | -0.011230 | -0.014270 | -0.017990 | -0.022260 | -0.024900 | -0.026740 | | |
| -0.028140 | -0.029260 | -0.030190 | -0.030980 | -0.031670 | -0.032270 | -0.032800 | -0.033250 | | |
| -0.033630 | -0.033950 | -0.034190 | -0.034360 | -0.034460 | -0.034470 | -0.034410 | -0.034260 | | |
| -0.034040 | -0.033730 | -0.033340 | -0.032860 | -0.032300 | -0.031670 | -0.030150 | -0.028330 | | |
| -0.026220 | -0.023840 | -0.022560 | -0.021220 | -0.019820 | -0.018370 | -0.016870 | -0.015320 | | |
| -0.013740 | -0.012110 | -0.010460 | -0.008770 | -0.007060 | -0.005330 | -0.003580 | -0.001830 | | |
| -0.000060 | 0.001710 | | | | | | | | |
| T | F | | | | | | | | |
| -0.009190 | -0.003000 | 0.000610 | 0.004520 | 0.010080 | 0.017870 | 0.023780 | 0.028650 | | |
| 0.032870 | 0.036590 | 0.039930 | 0.042940 | 0.045660 | 0.048100 | 0.050300 | 0.052260 | | |
| 0.053990 | 0.055500 | 0.056790 | 0.057880 | 0.058760 | 0.059440 | 0.059920 | 0.060220 | | |
| 0.060330 | 0.060260 | 0.060010 | 0.059600 | 0.059020 | 0.058280 | 0.056340 | 0.053840 | | |
| 0.050830 | 0.047350 | 0.045450 | 0.043470 | 0.041390 | 0.039230 | 0.037000 | 0.034710 | | |
| 0.032350 | 0.029940 | 0.027490 | 0.025000 | 0.022490 | 0.019940 | 0.017380 | 0.014810 | | |
| 0.012230 | 0.009650 | | | | | | | | |
| -0.009190 | -0.014990 | -0.018310 | -0.021310 | -0.024870 | -0.028830 | -0.031180 | -0.032780 | | |
| -0.033960 | -0.034880 | -0.035630 | -0.036260 | -0.036790 | -0.037220 | -0.037580 | -0.037860 | | |
| -0.038060 | -0.038180 | -0.038220 | -0.038180 | -0.038050 | -0.037840 | -0.037530 | -0.037150 | | |
| -0.036670 | -0.036100 | -0.035450 | -0.034700 | -0.033870 | -0.032960 | -0.030870 | -0.028460 | | |
| -0.025730 | -0.022720 | -0.021110 | -0.019430 | -0.017690 | -0.015900 | -0.014040 | -0.012140 | | |
| -0.010190 | -0.008200 | -0.006170 | -0.004100 | -0.002010 | 0.000110 | 0.002250 | 0.004400 | | |
| 0.006560 | 0.008730 | | | | | | | | |
| T | F | | | | | | | | |
| -0.019120 | -0.012950 | -0.009370 | -0.005400 | 0.000370 | 0.008440 | 0.014560 | 0.019630 | | |
| 0.024040 | 0.027960 | 0.031510 | 0.034740 | 0.037710 | 0.040430 | 0.042930 | 0.045210 | | |
| 0.047290 | 0.049170 | 0.050850 | 0.052350 | 0.053660 | 0.054790 | 0.055740 | 0.056520 | | |
| 0.057120 | 0.057550 | 0.057810 | 0.057910 | 0.057850 | 0.057640 | 0.056760 | 0.055310 | | |
| 0.053330 | 0.050870 | 0.049470 | 0.047960 | 0.046350 | 0.044660 | 0.042870 | 0.041010 | | |
| 0.039080 | 0.037080 | 0.035030 | 0.032920 | 0.030780 | 0.028600 | 0.026390 | 0.024160 | | |
| 0.021920 | 0.019680 | | | | | | | | |
| -0.019120 | -0.025250 | -0.028510 | -0.031390 | -0.034700 | -0.038160 | -0.040020 | -0.041170 | | |
| -0.041950 | -0.042510 | -0.042930 | -0.043220 | -0.043420 | -0.043530 | -0.043540 | -0.043470 | | |
| -0.043320 | -0.043080 | -0.042750 | -0.042340 | -0.041840 | -0.041250 | -0.040580 | -0.039820 | | |
| -0.038970 | -0.038030 | -0.037000 | -0.035880 | -0.034680 | -0.033380 | -0.030540 | -0.027350 | | |
| -0.023850 | -0.020030 | -0.018010 | -0.015920 | -0.013760 | -0.011540 | -0.009260 | -0.006920 | | |
| -0.004520 | -0.002080 | 0.000400 | 0.002920 | 0.005480 | 0.008060 | 0.010670 | 0.013290 | | |
| 0.015920 | 0.018560 | | | | | | | | |
| T | F | | | | | | | | |
| -0.034510 | -0.028160 | -0.024430 | -0.020280 | -0.014350 | -0.005910 | 0.000530 | 0.005870 | | |
| 0.010530 | 0.014700 | 0.018500 | 0.022000 | 0.025250 | 0.028270 | 0.031090 | 0.033730 | | |
| 0.036180 | 0.038470 | 0.040600 | 0.042560 | 0.044370 | 0.046020 | 0.047520 | 0.048870 | | |

| | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 0.050070 | 0.051120 | 0.052020 | 0.052780 | 0.053400 | 0.053880 | 0.054440 | 0.054490 |
| 0.054050 | 0.053170 | 0.052570 | 0.051870 | 0.051070 | 0.050190 | 0.049230 | 0.048200 |
| 0.047090 | 0.045920 | 0.044700 | 0.043430 | 0.042120 | 0.040780 | 0.039410 | 0.038020 |
| 0.036620 | 0.035210 | | | | | | |
| -0.034510 | -0.040970 | -0.044000 | -0.046630 | -0.049350 | -0.051350 | -0.051670 | -0.051490 |
| -0.051150 | -0.050760 | -0.050360 | -0.049950 | -0.049510 | -0.049030 | -0.048510 | -0.047930 |
| -0.047290 | -0.046580 | -0.045800 | -0.044950 | -0.044010 | -0.042990 | -0.041870 | -0.040670 |
| -0.039380 | -0.037990 | -0.036500 | -0.034920 | -0.033240 | -0.031470 | -0.027630 | -0.023410 |
| -0.018840 | -0.013920 | -0.011350 | -0.008690 | -0.005970 | -0.003170 | -0.000310 | 0.002610 |
| 0.005580 | 0.008590 | 0.011660 | 0.014750 | 0.017880 | 0.021040 | 0.024210 | 0.027400 |
| 0.030600 | 0.033800 | | | | | | |

*** END OF AIRFOIL DATA ***

F14 PLANFORM DESCRIPTION

| | | | | | |
|-----------|-------|-----------|-----------|-----------|-----------|
| 0.0 | 0.0 | 167.20971 | 384.69995 | 140.06494 | 184.32837 |
| 40676.853 | 160.0 | 76.00073 | | | |

1

2

| | | | |
|------------|------------|-----------|-----------|
| 0.0 | 0.0 | 384.69995 | 140.06494 |
| .364088792 | .364088792 | | |

1

2

| | | | |
|------------|------------|-----------|-----------|
| 0.0 | 167.20971 | 384.69995 | 184.32837 |
| .047914841 | .047914841 | | |

| | | | | | | | |
|--------|-----|---------|-----|--------|-----|--------|-----|
| 0.0 | 0.0 | .330725 | 0.0 | .42634 | 0.0 | .52196 | 0.0 |
| .61758 | 0.0 | .71320 | 0.0 | .80882 | 0.0 | .90444 | 0.0 |

1.0 0.0

45X30X16 MESH

```
&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,ISHEAR=0,NTIPLE=1&END
&XGRID NXON=25,NXFWD=10,NXAFT=10,XFWD=-5.0,XAFT=8.0&END
&YGRID NYON=20,NYOFF=10,YMAX=2.0&END
&ZGRID NZ=16,ZP=1.75,ZMAX=5.0&END
&SOLVIN MACH=.80,AOA=1.4,NGSEQ=2,MAXIT=300,RCONV=.001,
      OMEGX=1.80,OMEGY=1.80,OMEZ=1.80,OMEGG=1.2,
      IPRINT=0,IPLOT=0,ICIRPF=100,IKLUNK=1,
      CON=1.0,BXI=0.0&END
```

90X30X30 MESH

```
&GPARM IPRNTG=0&END
&XGRID NXON=50.NXFWD=20,NXAFT=20&END
&YGRID NYON=20,NYOFF=10&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=300,RCONV=.001,IPRINT=1,IPLOT=1,ICIRPF=300,
      OMEGX=1.8,OMEGY=1.8,OMEZ=1.8,OMEGG=1.2&END
```

SAMPLE DATA SET NO. 5
WING A VISCOUS ANALYSIS

WING A VISCOUS ANALYSIS

MACH=0.80 AOA=1.2

WINGA ORDINATES

| | 2 | 33 | 33 | 0 | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.002408 | 0.009607 | 0.021530 | 0.038060 | 0.059039 | 0.084265 | 0.113495 | |
| 0.146447 | 0.182803 | 0.222215 | 0.264302 | 0.308658 | 0.354858 | 0.402455 | 0.450991 | |
| 0.500000 | 0.549009 | 0.597545 | 0.645142 | 0.691342 | 0.735698 | 0.777785 | 0.817197 | |
| 0.853553 | 0.886505 | 0.915735 | 0.940961 | 0.961940 | 0.978470 | 0.990393 | 0.997592 | |
| 1.000000 | | | | | | | | |
| 0.000000 | 0.002408 | 0.009607 | 0.021530 | 0.038060 | 0.059039 | 0.084265 | 0.113495 | |
| 0.146447 | 0.182803 | 0.222215 | 0.264302 | 0.308658 | 0.354858 | 0.402455 | 0.450991 | |
| 0.500000 | 0.549009 | 0.597545 | 0.645142 | 0.691342 | 0.735698 | 0.777785 | 0.817197 | |
| 0.853553 | 0.886505 | 0.915735 | 0.940961 | 0.961940 | 0.978470 | 0.990393 | 0.997592 | |
| 1.000000 | | | | | | | | |
| 0.000000 | 0.009523 | 0.017576 | 0.024310 | 0.030180 | 0.034958 | 0.038571 | 0.041361 | |
| 0.043645 | 0.045539 | 0.047036 | 0.048065 | 0.048637 | 0.048737 | 0.048351 | 0.047358 | |
| 0.045740 | 0.043449 | 0.040624 | 0.037256 | 0.033534 | 0.029576 | 0.025544 | 0.021533 | |
| 0.017667 | 0.014102 | 0.010867 | 0.008059 | 0.005745 | 0.003816 | 0.002366 | 0.001245 | |
| 0.000801 | | | | | | | | |
| 0.000000 | -0.007998 | -0.015781 | -0.022051 | -0.028216 | -0.034320 | -0.040552 | -0.046841 | |
| -0.053095 | -0.058886 | -0.063909 | -0.067723 | -0.070312 | -0.071256 | -0.070937 | -0.068816 | |
| -0.065403 | -0.060078 | -0.053487 | -0.045480 | -0.036948 | -0.028384 | -0.020344 | -0.013234 | |
| -0.007335 | -0.002835 | 0.000160 | 0.001680 | 0.001953 | 0.001417 | 0.000485 | -0.000425 | |
| -0.000803 | | | | | | | | |

| T | F | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.007883 | 0.016974 | 0.025572 | 0.033052 | 0.039841 | 0.046100 | 0.051716 | |
| 0.056576 | 0.060668 | 0.064013 | 0.066654 | 0.068589 | 0.069825 | 0.070362 | 0.070214 | |
| 0.069431 | 0.067991 | 0.065908 | 0.063109 | 0.059558 | 0.055045 | 0.049478 | 0.042953 | |
| 0.035847 | 0.028744 | 0.022061 | 0.016177 | 0.011340 | 0.007448 | 0.004805 | 0.002848 | |
| 0.002073 | | | | | | | | |
| 0.000000 | -0.008988 | -0.015880 | -0.021410 | -0.025889 | -0.029641 | -0.033196 | -0.036588 | |
| -0.039898 | -0.042959 | -0.045616 | -0.047750 | -0.049215 | -0.049918 | -0.049642 | -0.048016 | |
| -0.044596 | -0.039227 | -0.032380 | -0.024781 | -0.017099 | -0.009966 | -0.003808 | 0.000991 | |
| 0.004231 | 0.005957 | 0.006171 | 0.005222 | 0.003575 | 0.001547 | -0.000032 | -0.001456 | |
| -0.002070 | | | | | | | | |

*** END OF WINGA AIRFOIL DATA ***

WINGA PLANFORM DESCRIPTION

| | | | | | |
|---------|---------|--------|----------|---------|----------|
| 0.0 | 0.0 | 6.500 | 18.00000 | 9.36853 | 11.96853 |
| 81.8 | 4.825 | 5.221 | | | |
| | 1 | | | | |
| | 2 | | | | |
| 0.0 | 0.0 | 18.000 | 9.36853 | | |
| .520474 | .520474 | | | | |

```

1
2
0.0      6.5      18.000    11.96853
.303808   .303808
0.0      2.57     1.0       -2.00
25X30X8 GRID
&GPARM IPRNTG=0,WBCPRT=.F.,ISAMG=1,NTIPLE=1&END
&XGRID NXON=10,NXFWD=7,NXAFT=8,XFWD=-5.0,XAFT=8.0&END
&YGRID NYON=20,NYOFF=10,YMAX=2.0&END
&ZGRID NZ=8,ZP=3.3&END
&SOLVIN MACH=0.80,AOA=1.2,MAXIT=400,OMEGX=1.92,
          OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=100,
          OMEGZ=1.92,CON=1.0,NGSEQ=3,BXI=0.0,
          IPLOT=0,IPU=8.0MEGG=1.2,IKLUNK=1,IDESN=0&END
45X30X16 GRID
&GPARM IPRNTG=0,WBCPRT=.F.&END
&XGRID NXON=25,NXFWD=10,NXAFT=10&END
&YGRID NYON=20.NYOFF=10&END
&ZGRID NZ=16,ZP=1.75,ZMAX=5.0&END
&SOLVIN MAXIT=400,OMEGX=1.95,OMEGY=1.95,RCONV=.0001,IPRINT=0,
          ICIRPF=100,OMEGZ=1.95,CON=1.0,BXI=0.0,IVISC=1,
          IPLOT=0,IPU=8,OMEgg=1.2&END
&VISCDT ITR=10,NVISC=100,NPRV=401,NJPRV=9,RN=8080000.,
          DELCOR=.82139&END
90X30X30 GRID
&GPARM IPRNTG=0,WBCPRT=.F.&END
&XGRID NXON=50,NXFWD=20,NXAFT=20&END
&YGRID NYON=20,NYOFF=10&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=400,OMEGX=1.95,
          OMEGY=1.95,RCONV=.0001,IPRINT=1,ICIRPF=50,
          OMEGZ=1.95,IPLOT=1,IPU=8,OMEgg=1.2,IKLUNK=1,
          BXI=0.0,CON=1.0&END
&VISCDT ITR=10,NVISC=100,NPRV=400,NJPRV=9&END

```

SAMPLE DATA SET NO. 6
WING C INVISCID ANALYSIS

WING C INVISCID ANALYSIS

MACH=0.83 AOA=5.0

WING C ORDINATES

| | 2 | 33 | 33 | 0 | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.002408 | 0.009607 | 0.021530 | 0.038060 | 0.059039 | 0.084265 | 0.113495 | |
| 0.146447 | 0.182803 | 0.222215 | 0.264302 | 0.308658 | 0.354858 | 0.402455 | 0.450991 | |
| 0.500000 | 0.549009 | 0.597545 | 0.645142 | 0.691342 | 0.735698 | 0.777785 | 0.817197 | |
| 0.853553 | 0.886505 | 0.915735 | 0.940961 | 0.961940 | 0.978470 | 0.990393 | 0.997592 | |
| 1.000000 | | | | | | | | |
| 0.000000 | 0.002408 | 0.009607 | 0.021530 | 0.038060 | 0.059039 | 0.084265 | 0.113495 | |
| 0.146447 | 0.182803 | 0.222215 | 0.264302 | 0.308658 | 0.354858 | 0.402455 | 0.450991 | |
| 0.500000 | 0.549009 | 0.597545 | 0.645142 | 0.691342 | 0.735698 | 0.777785 | 0.817197 | |
| 0.853553 | 0.886505 | 0.915735 | 0.940961 | 0.961940 | 0.978470 | 0.990393 | 0.997592 | |
| 1.000000 | | | | | | | | |
| 0.000000 | 0.007078 | 0.015211 | 0.022409 | 0.028113 | 0.032665 | 0.036344 | 0.039106 | |
| 0.040977 | 0.042046 | 0.042446 | 0.042381 | 0.041875 | 0.040963 | 0.039692 | 0.038005 | |
| 0.036025 | 0.033750 | 0.031266 | 0.028567 | 0.025780 | 0.022922 | 0.020008 | 0.017060 | |
| 0.014113 | 0.011218 | 0.008528 | 0.006165 | 0.004213 | 0.002720 | 0.001669 | 0.001034 | |
| 0.000820 | | | | | | | | |
| 0.000000 | -0.006221 | -0.009909 | -0.012680 | -0.015584 | -0.018603 | -0.021094 | -0.023104 | |
| -0.024642 | -0.025693 | -0.026348 | -0.026447 | -0.026081 | -0.025220 | -0.024010 | -0.022330 | |
| -0.020180 | -0.017188 | -0.013545 | -0.009434 | -0.005720 | -0.002752 | -0.000712 | 0.000412 | |
| 0.000767 | 0.000537 | 0.000118 | -0.000285 | -0.000557 | -0.000575 | -0.000695 | -0.000791 | |
| -0.000823 | | | | | | | | |

| T | F | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|
| 0.000000 | 0.005979 | 0.014276 | 0.022373 | 0.030131 | 0.037796 | 0.045339 | 0.052724 | |
| 0.059929 | 0.066822 | 0.073148 | 0.078516 | 0.082519 | 0.084923 | 0.085600 | 0.084549 | |
| 0.081909 | 0.077914 | 0.072839 | 0.066913 | 0.060301 | 0.053236 | 0.046023 | 0.038892 | |
| 0.032028 | 0.025650 | 0.019838 | 0.014702 | 0.010355 | 0.006916 | 0.004546 | 0.003161 | |
| 0.002704 | | | | | | | | |
| 0.000000 | -0.008265 | -0.012773 | -0.015803 | -0.018133 | -0.020204 | -0.021813 | -0.023033 | |
| -0.023855 | -0.024169 | -0.024120 | -0.023592 | -0.022620 | -0.021102 | -0.019120 | -0.016540 | |
| -0.013462 | -0.009562 | -0.005017 | -0.000128 | 0.004105 | 0.007319 | 0.009262 | 0.009845 | |
| 0.009212 | 0.007659 | 0.005620 | 0.003410 | 0.001300 | -0.000327 | -0.001630 | -0.002422 | |
| -0.002681 | | | | | | | | |

*** END OF WING C AIRFOIL DATA ***

WINGC PLANFORM DESCRIPTION

| | | | | | |
|-----|-----|--------|----------|----------|-------|
| 0.0 | 0.0 | 12.140 | 10.26000 | 10.26000 | 13.90 |
|-----|-----|--------|----------|----------|-------|

| | | | | | |
|------|-------|-------|--|--|--|
| 81.0 | 8.642 | 6.367 | | | |
|------|-------|-------|--|--|--|

1

2

| | | | | | |
|-----|-----|--------|-------|--|--|
| 0.0 | 0.0 | 10.260 | 10.26 | | |
|-----|-----|--------|-------|--|--|

1.0 1.0
1
2
0.0 12.14 10.260 13.90
.171539961.171539961
0.0 2.39 1.0 -5.59
26X30X8 GRID
&GPARM WBCPRT=.F.,NTIPLE=1&END
&XGRID XFWD=-5.0,XAFT=8.0,NXON=10,NXFWD=8,NXAFT=8&END
&YGRID NYON=20,NYOFF=10,YMAX=1.4&END
&ZGRID NZ=8,ZP=3.3&END
&SOLVIN MACH=0.83,AOA=5.0,MAXIT=400,OMEGX=1.92,IKLUNK=1,
OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=100,
OMEGZ=1.92,NGSEQ=3,IPLT=0,IPU=8,OME GG=1.2&END
45X30X16 GRID
&GPARM WBCPRT=.F.&END
&XGRID NXON=25,NXFWD=10,NXAFT=10&END
&YGRID NYON=20,NYOFF=10&END
&ZGRID NZ=16,ZMAX=5.0&END
&SOLVIN MAXIT=400,OMEGX=1.9,OMEGY=1.9,RCONV=.0001,
IPRINT=1,ICIRPF=100,OMEGZ=1.9&END
90X30X30 GRID
&GPARM IPRNTG=0,WBCPRT=.F.&END
&XGRID NXON=50,NXFWD=20,NXAFT=20&END
&YGRID NYON=20,NYOFF=10&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=100,OMEGX=1.75,OMEGY=1.75,RCONV=.001,
IPRINT=1,ICIRPF=50,OMEGZ=1.75,IPLT=1&END

APPENDIX B
SAMPLE OUTPUT

The following pages illustrate the major blocks of data that are printed during the course of an analysis or design run.

TEST CASE DESCRIPTION

M6 VISCOUS INV VISC TARG WITH MODIFIED CPS wJ 12 JD 12.12
ZEBIPLS VERS OF CODE CORRECTED SHAPE DTETW .01 MAXIT 400

... AIRFOIL ORDINATES INPUT FROM UNIT S ...

... END OF SECTION DATA ...

ONERA M6 PLANFORM DESCRIPTION

YROOT XTER XTER YTER XTER XTER YTER

0 0000 0 0000 805 90001196 3000 690 68411143 5999

SREF CREF XMOM

752960 1 646 0700 201 4750

NLES 1

NLEI 2

YLEI XLEI

0 0000 0 0000

1196 3000 690 6841

DXLER DXLET

0 577350 0 577350

NTES 1

NTEI 1

YTEI XTEI

0 0000 805 9000

1196 3000 1143 5999

DXTER DXLET

0 282971 0 282971

NPAN INU INL KSMTHS

4 69 69 0

N YF(N) THETP(N)

1 0 000000 0 000000

2 0 200000 0 000000

3 0 600000 0 000000

4 0 999990 0 000000

PLANFORM INPUT DESCRIPTION

| X | C | AT WHICH | UPPER SURFACE | ORDINATES | ARE INPUT |
|------------------------------|----------|----------|---------------|-----------|-----------|
| 0 | 0.00000 | 0 | 0.00323 | 0 | 0.00551 |
| 0 | 0.004570 | 0 | 0.005975 | 0 | 0.007711 |
| 0 | 0.029701 | 0 | 0.036426 | 0 | 0.044485 |
| 0 | 0.137896 | 0 | 0.164998 | 0 | 0.191953 |
| 0 | 0.350283 | 0 | 0.378145 | 0 | 0.401857 |
| 0 | 0.553094 | 0 | 0.577804 | 0 | 0.602376 |
| 0 | 0.746986 | 0 | 0.770800 | 0 | 0.794106 |
| 0 | 0.922534 | 0 | 0.936335 | 0 | 0.947995 |
| 0 | 0.988525 | 0 | 0.992144 | 0 | 0.995208 |
| Y(N) | 0 | 0.000000 | | | |
| X | C | AT WHICH | LOWER SURFACE | ORDINATES | ARE INPUT |
| 0 | 0.00000 | 0 | 0.00323 | 0 | 0.00551 |
| 0 | 0.004570 | 0 | 0.005975 | 0 | 0.007711 |
| 0 | 0.029701 | 0 | 0.036426 | 0 | 0.044485 |
| 0 | 0.137896 | 0 | 0.164998 | 0 | 0.191953 |
| 0 | 0.350283 | 0 | 0.378145 | 0 | 0.401857 |
| 0 | 0.553094 | 0 | 0.577804 | 0 | 0.602376 |
| 0 | 0.746986 | 0 | 0.770800 | 0 | 0.794106 |
| 0 | 0.922534 | 0 | 0.936335 | 0 | 0.947995 |
| 0 | 0.988525 | 0 | 0.992144 | 0 | 0.995208 |
| Y(N) | 0 | 0.000000 | | | |
| THE FOLLOWING ZU C ARE INPUT | | | | | |
| 0 | 0.00000 | 0 | 0.003138 | 0 | 0.004096 |
| 0 | 0.011742 | 0 | 0.013371 | 0 | 0.015095 |
| 0 | 0.025825 | 0 | 0.027332 | 0 | 0.028791 |
| 0 | 0.039852 | 0 | 0.041909 | 0 | 0.043621 |
| 0 | 0.048818 | 0 | 0.048930 | 0 | 0.048820 |
| 0 | 0.043674 | 0 | 0.042168 | 0 | 0.040524 |
| 0 | 0.028737 | 0 | 0.026550 | 0 | 0.024303 |
| 0 | 0.010273 | 0 | 0.008583 | 0 | 0.007142 |
| 0 | 0.002126 | 0 | 0.001678 | 0 | 0.001298 |
| Y(N) | 0 | 0.000000 | | | |
| THE FOLLOWING ZL C ARE INPUT | | | | | |
| 0 | 0.00000 | 0 | 0.003138 | 0 | 0.004096 |
| 0 | 0.011742 | 0 | 0.013371 | 0 | 0.015095 |
| 0 | 0.025825 | 0 | 0.027332 | 0 | 0.028791 |
| 0 | 0.039852 | 0 | 0.041909 | 0 | 0.043621 |
| 0 | 0.048818 | 0 | 0.048930 | 0 | 0.048820 |
| 0 | 0.043674 | 0 | 0.042168 | 0 | 0.040524 |
| 0 | 0.028737 | 0 | 0.026550 | 0 | 0.024303 |
| 0 | 0.010273 | 0 | 0.008583 | 0 | 0.007142 |
| 0 | 0.002126 | 0 | 0.001678 | 0 | 0.001298 |

| X | C | AT WHICH | UPPER SURFACE | ORDINATES | ARE INPUT |
|------------------------------|----------|----------|---------------|-----------|-----------|
| 0 | 0.00000 | 0 | 0.00323 | 0 | 0.00551 |
| 0 | 0.004570 | 0 | 0.005975 | 0 | 0.007711 |
| 0 | 0.029701 | 0 | 0.036426 | 0 | 0.044485 |
| 0 | 0.137896 | 0 | 0.164998 | 0 | 0.191953 |
| 0 | 0.350283 | 0 | 0.378145 | 0 | 0.401857 |
| 0 | 0.553094 | 0 | 0.577804 | 0 | 0.602376 |
| 0 | 0.746986 | 0 | 0.770800 | 0 | 0.794106 |
| 0 | 0.922534 | 0 | 0.936335 | 0 | 0.947995 |
| 0 | 0.988525 | 0 | 0.992144 | 0 | 0.995208 |
| Y(N) | 0 | 0.000000 | | | |
| X | C | AT WHICH | LOWER SURFACE | ORDINATES | ARE INPUT |
| 0 | 0.00000 | 0 | 0.00323 | 0 | 0.00551 |
| 0 | 0.004570 | 0 | 0.005975 | 0 | 0.007711 |
| 0 | 0.029701 | 0 | 0.036426 | 0 | 0.044485 |
| 0 | 0.137896 | 0 | 0.164998 | 0 | 0.191953 |
| 0 | 0.350283 | 0 | 0.378145 | 0 | 0.401857 |
| 0 | 0.553094 | 0 | 0.577804 | 0 | 0.602376 |
| 0 | 0.746986 | 0 | 0.770800 | 0 | 0.794106 |
| 0 | 0.922534 | 0 | 0.936335 | 0 | 0.947995 |
| 0 | 0.988525 | 0 | 0.992144 | 0 | 0.995208 |
| Y(N) | 0 | 0.000000 | | | |
| THE FOLLOWING ZU C ARE INPUT | | | | | |
| 0 | 0.00000 | 0 | 0.003138 | 0 | 0.004096 |
| 0 | 0.011742 | 0 | 0.013371 | 0 | 0.015095 |
| 0 | 0.025825 | 0 | 0.027332 | 0 | 0.028791 |
| 0 | 0.039852 | 0 | 0.041909 | 0 | 0.043621 |
| 0 | 0.048818 | 0 | 0.048930 | 0 | 0.048820 |
| 0 | 0.043674 | 0 | 0.042168 | 0 | 0.040524 |
| 0 | 0.028737 | 0 | 0.026550 | 0 | 0.024303 |
| 0 | 0.010273 | 0 | 0.008583 | 0 | 0.007142 |
| 0 | 0.002126 | 0 | 0.001678 | 0 | 0.001298 |
| THE FOLLOWING ZL C ARE INPUT | | | | | |
| 0 | 0.00000 | 0 | 0.003138 | 0 | 0.004096 |
| 0 | 0.011742 | 0 | 0.013371 | 0 | 0.015095 |
| 0 | 0.025825 | 0 | 0.027332 | 0 | 0.028791 |
| 0 | 0.039852 | 0 | 0.041909 | 0 | 0.043621 |
| 0 | 0.048818 | 0 | 0.048930 | 0 | 0.048820 |
| 0 | 0.043674 | 0 | 0.042168 | 0 | 0.040524 |
| 0 | 0.028737 | 0 | 0.026550 | 0 | 0.024303 |
| 0 | 0.010273 | 0 | 0.008583 | 0 | 0.007142 |
| 0 | 0.002126 | 0 | 0.001678 | 0 | 0.001298 |

COARSE SKEWED MESH

| | | | | |
|------|-------|-------|--------|--------|
| NXON | NXFWD | NXAFT | XPLE | XPTE |
| 10 | 7 | 8 | 0 2000 | 0 2000 |

| | | | |
|------|-------|-------|------|
| NYON | NYOFF | YPTIP | |
| 20 | 10 | 1 | 3000 |

NZ 2P

```

8 3 6550
$SOLVIN MAXIT 200. OMEGX 1.92. OMEGY 1.92. OMEGZ 1.92. NI 90. NJ 30. RCONV 1.E 5. BXI 0.
AOA 3.06. MACH 0. 8355. IPRINT 0. IPLOT 0. ISDBC 0. NDIF 0. NITRL 100. SRMAX 2.1. BMAX 2.
CON 1. IDESN 0. IOPT 0. IPRSHF 0. IRLOFT 0. IVISIC 0. ICPSDC 0. OMEGG 0. OMEGS 0. ICIRPF 100. IKLUNK 1.
NGSEQ 3. IPU 8. NITRF 10. ITED 0. ILED 0. NIIDSN 0. ISVSHP 0. INV 0. INVM 0. INVR 0. INVS 0. INVSHP 5.
ISRLOR 0. IFSHPP 100. &END

```

INPUT REQUIRED 0.0227 CPU SECONDS

```

XPLE 1.860148 XPTE 1 585522
YP 1.241286

```

MESH GENERATION DATA

WING DESCRIPTION

| L E | T E | ROOT CHORD | TIP CHORD | WING AREA | ASPECT RATIO | TAPER RATIO | REF CHORD |
|-----------------|--------|------------|-----------|-----------|--------------|-------------|-----------|
| SWEET 0 5774 | 0 2823 | 1 0000 | 0 5620 | 1 159 | 3 8014 | 0 5620 | 0 8017 |

WING LEADING AND TRAILING EDGE COORDINATES

XLEW XTEW

| K | ETA | NOMINAL WING ROOT | WING | ASPECT | TAPER | REF |
|----|----------|-------------------|-----------|-----------|-----------|-----------|
| 1 | 0 00000 | 0 000000 | 1 000000 | 1 000000 | 1 000000 | 1 000000 |
| 2 | 0 076124 | 0 043950 | 1 021533 | 1 021533 | 1 021533 | 1 021533 |
| 3 | 0 152249 | 0 087901 | 1 043052 | 1 043052 | 1 043052 | 1 043052 |
| 4 | 0 228373 | 0 131651 | 1 064558 | 1 064558 | 1 064558 | 1 064558 |
| 5 | 0 304498 | 0 175802 | 1 088054 | 1 088054 | 1 088054 | 1 088054 |
| 6 | 0 380622 | 0 219752 | 1 107539 | 1 107539 | 1 107539 | 1 107539 |
| 7 | 0 456747 | 0 261703 | 1 129017 | 1 129017 | 1 129017 | 1 129017 |
| 8 | 0 532871 | 0 307653 | 1 150489 | 1 150489 | 1 150489 | 1 150489 |
| 9 | 0 608996 | 0 351604 | 1 171956 | 1 171956 | 1 171956 | 1 171956 |
| 10 | 0 685120 | 0 395554 | 1 193420 | 1 193420 | 1 193420 | 1 193420 |
| 11 | 0 761245 | 0 439505 | 1 214883 | 1 214883 | 1 214883 | 1 214883 |
| 12 | 0 837369 | 0 483555 | 1 236346 | 1 236346 | 1 236346 | 1 236346 |
| 13 | 0 913494 | 0 527408 | 1 257812 | 1 257812 | 1 257812 | 1 257812 |
| 14 | 0 989618 | 0 571356 | 1 279281 | 1 279281 | 1 279281 | 1 279281 |
| 15 | 0 865743 | 0 615307 | 1 300756 | 1 300756 | 1 300756 | 1 300756 |
| 16 | 1 141867 | 0 659557 | 1 322237 | 1 322237 | 1 322237 | 1 322237 |
| 17 | 1 217992 | 0 703208 | 1 343727 | 1 343727 | 1 343727 | 1 343727 |
| 18 | 1 284116 | 0 747158 | 1 365228 | 1 365228 | 1 365228 | 1 365228 |
| 19 | 1 370241 | 0 791109 | 1 3886740 | 1 3886740 | 1 3886740 | 1 3886740 |
| 20 | 1 446365 | 0 835659 | 1 4082266 | 1 4082266 | 1 4082266 | 1 4082266 |

XI-O AND XI-1 COORDINATES AND SLOPES

| K | ETA | XI-O XLE | XI-1 XTE | XLEP | XTEP |
|----|----------|----------|-----------|----------|----------|
| 1 | 0 00000 | 0 000000 | 1 000000 | 0 577350 | 0 577350 |
| 2 | 0 076124 | 0 043950 | 1 021533 | 0 577350 | 0 577350 |
| 3 | 0 152249 | 0 087901 | 1 043052 | 0 577350 | 0 577350 |
| 4 | 0 228373 | 0 131651 | 1 064558 | 0 577350 | 0 577350 |
| 5 | 0 304498 | 0 175802 | 1 088054 | 0 577350 | 0 577350 |
| 6 | 0 380622 | 0 219752 | 1 107539 | 0 577350 | 0 577350 |
| 7 | 0 456747 | 0 261703 | 1 129017 | 0 577350 | 0 577350 |
| 8 | 0 532871 | 0 307653 | 1 150489 | 0 577350 | 0 577350 |
| 9 | 0 608996 | 0 351604 | 1 171956 | 0 577350 | 0 577350 |
| 10 | 0 685120 | 0 395554 | 1 193420 | 0 577350 | 0 577350 |
| 11 | 0 761245 | 0 439505 | 1 214883 | 0 577350 | 0 577350 |
| 12 | 0 837369 | 0 483455 | 1 236346 | 0 577350 | 0 577350 |
| 13 | 0 913494 | 0 527408 | 1 257812 | 0 577350 | 0 577350 |
| 14 | 0 989618 | 0 571356 | 1 279281 | 0 577350 | 0 577350 |
| 15 | 1 065743 | 0 615307 | 1 300756 | 0 577350 | 0 577350 |
| 16 | 1 141867 | 0 659267 | 1 322237 | 0 577350 | 0 577350 |
| 17 | 1 217992 | 0 703208 | 1 343727 | 0 577350 | 0 577350 |
| 18 | 1 284116 | 0 747158 | 1 365228 | 0 577350 | 0 577350 |
| 19 | 1 370241 | 0 791109 | 1 3886740 | 0 577350 | 0 577350 |

COMPUTED PLANFORM DATA

| K | ETA NOMINAL WING ROOT | J INDEX WING TIP | JLE JTE | DX (X XTEW), C | DX (X XTEW), C |
|----|-----------------------------|---------------------|------------|-------------------|-------------------|
| 1 | 0 000000 | 8 | 17 | 0 052632 | 1 000000 |
| 2 | 0 076124 | 8 | 17 | 0 052632 | 1 000000 |
| 3 | 0 152249 | 8 | 17 | 0 052632 | 1 000000 |
| 4 | 0 228373 | 8 | 17 | 0 052632 | 1 000000 |
| 5 | 0 304498 | 8 | 17 | 0 052632 | 1 000000 |
| 6 | 0 380622 | 8 | 17 | 0 052632 | 1 000000 |
| 7 | 0 456747 | 8 | 17 | 0 052632 | 1 000000 |
| 8 | 0 532871 | 8 | 17 | 0 052632 | 1 000000 |
| 9 | 0 608996 | 8 | 17 | 0 052632 | 1 000000 |
| 10 | 0 685120 | 8 | 17 | 0 052632 | 1 000000 |
| 11 | 0 761245 | 8 | 17 | 0 052632 | 1 000000 |
| 12 | 0 837369 | 8 | 17 | 0 052632 | 1 000000 |
| 13 | 0 913494 | 8 | 17 | 0 052632 | 1 000000 |
| 14 | 0 989618 | 8 | 17 | 0 052632 | 1 000000 |
| 15 | 1 065743 | 8 | 17 | 0 052632 | 1 000000 |
| 16 | 1 141867 | 8 | 17 | 0 052632 | 1 000000 |
| 17 | 1 217992 | 8 | 17 | 0 052632 | 1 000000 |
| 18 | 1 294116 | 8 | 17 | 0 052632 | 1 000000 |
| 19 | 1 370241 | 8 | 17 | 0 052632 | 1 000000 |
| 20 | 1 446365 | 8 | 17 | 0 052632 | 1 000000 |

J INDEX OF LEADING AND TRAILING EDGE POINTS AND DX C

| K | ETA NOMINAL WING ROOT | JLE | JTE | DX (X XTEW), C | DX (X XTEW), C |
|----|-----------------------------|-----|-----|-------------------|-------------------|
| 1 | 0 000000 | 8 | 17 | 0 052632 | 1 000000 |
| 2 | 0 076124 | 8 | 17 | 0 052632 | 1 000000 |
| 3 | 0 152249 | 8 | 17 | 0 052632 | 1 000000 |
| 4 | 0 228373 | 8 | 17 | 0 052632 | 1 000000 |
| 5 | 0 304498 | 8 | 17 | 0 052632 | 1 000000 |
| 6 | 0 380622 | 8 | 17 | 0 052632 | 1 000000 |
| 7 | 0 456747 | 8 | 17 | 0 052632 | 1 000000 |
| 8 | 0 532871 | 8 | 17 | 0 052632 | 1 000000 |
| 9 | 0 608996 | 8 | 17 | 0 052632 | 1 000000 |
| 10 | 0 685120 | 8 | 17 | 0 052632 | 1 000000 |
| 11 | 0 761245 | 8 | 17 | 0 052632 | 1 000000 |
| 12 | 0 837369 | 8 | 17 | 0 052632 | 1 000000 |
| 13 | 0 913494 | 8 | 17 | 0 052632 | 1 000000 |
| 14 | 0 989618 | 8 | 17 | 0 052632 | 1 000000 |
| 15 | 1 065743 | 8 | 17 | 0 052632 | 1 000000 |
| 16 | 1 141867 | 8 | 17 | 0 052632 | 1 000000 |
| 17 | 1 217992 | 8 | 17 | 0 052632 | 1 000000 |
| 18 | 1 294116 | 8 | 17 | 0 052632 | 1 000000 |
| 19 | 1 370241 | 8 | 17 | 0 052632 | 1 000000 |
| 20 | 1 446365 | 8 | 17 | 0 052632 | 1 000000 |

MESH GENERATION REQUIRED 0.11502 CPU SECONDS

NI NJ NK KUP ILE ITE JTIP
25 30 8 5 8 17 21

RHOINF QINF
0.71917 0.86095

INITIALIZATION REQUIRED 0.0016 CPU SECONDS

| NIT | IChAX | JChAX | KChAX | ChAX | JRMAX | KRMAX | RMAX | RAVG |
|-----|-------|-------|-------|-------------|-------|-------|------|--------------|
| 1 | 17 | 1 | 5 | 0.82328E-02 | 17 | 1 | 5 | 0.17664E-01 |
| 2 | 17 | 1 | 5 | 0.11550E-01 | 17 | 1 | 5 | 0.25099E-01 |
| 3 | 18 | 2 | 5 | 0.11583E-01 | 18 | 2 | 5 | 0.23272E-01 |
| 4 | 19 | 2 | 5 | 0.11189E-01 | 19 | 2 | 5 | 0.18050E-01 |
| 5 | 19 | 4 | 5 | 0.71022E-02 | 17 | 4 | 5 | 0.13710E-01 |
| 6 | 16 | 8 | 5 | 0.49156E-02 | 17 | 6 | 5 | 0.10555E-01 |
| 7 | 16 | 8 | 5 | 0.40189E-02 | 16 | 8 | 5 | 0.83312E-00 |
| 8 | 21 | 9 | 5 | 0.41465E-02 | 15 | 10 | 5 | 0.69460E-00 |
| 9 | 20 | 3 | 6 | 0.39641E-02 | 15 | 10 | 5 | 0.59061E-00 |
| 10 | 21 | 1 | 6 | 0.36226E-02 | 17 | 7 | 6 | 0.52704E-00 |
| 11 | 21 | 3 | 6 | 0.34110E-02 | 17 | 9 | 6 | 0.50970E-00 |
| 12 | 21 | 3 | 6 | 0.28202E-02 | 17 | 9 | 6 | 0.48117E-00 |
| 13 | 21 | 3 | 5 | 0.32721E-02 | 21 | 5 | 5 | 0.49367E-00 |
| 14 | 21 | 4 | 5 | 0.26567E-02 | 16 | 8 | 6 | 0.40307E-00 |
| 15 | 16 | 11 | 6 | 0.19872E-02 | 16 | 9 | 6 | 0.37850E-00 |
| 16 | 15 | 11 | 6 | 0.18454E-02 | 17 | 5 | 5 | 0.36854E-00 |
| 17 | 22 | 5 | 5 | 0.25184E-02 | 22 | 5 | 5 | 0.37184E-00 |
| 18 | 22 | 2 | 5 | 0.25922E-02 | 22 | 2 | 5 | 0.38835E-00 |
| 19 | 17 | 2 | 5 | 0.15576E-02 | 17 | 2 | 5 | 0.35076E-00 |
| 20 | 16 | 4 | 5 | 0.15122E-02 | 17 | 2 | 5 | 0.33872E-00 |
| 21 | 16 | 4 | 5 | 0.14787E-02 | 17 | 2 | 5 | 0.32403E-00 |
| 22 | 22 | 2 | 4 | 0.18916E-02 | 17 | 2 | 5 | 0.30584E-00 |
| 23 | 24 | 3 | 4 | 0.16307E-02 | 16 | 2 | 5 | 0.29219E-00 |
| 24 | 15 | 6 | 5 | 0.13613E-02 | 15 | 6 | 5 | 0.27814E-00 |
| 25 | 14 | 8 | 5 | 0.13361E-02 | 15 | 6 | 5 | 0.26628E-00 |
| 26 | 22 | 1 | 5 | 0.13043E-02 | 14 | 8 | 5 | 0.25555E-00 |
| 27 | 22 | 2 | 5 | 0.14550E-02 | 14 | 8 | 5 | 0.245555E-00 |
| 28 | 12 | 5 | 5 | 0.11998E-02 | 14 | 8 | 5 | 0.23364E-00 |
| 29 | 13 | 12 | 5 | 0.11477E-02 | 14 | 6 | 5 | 0.22114E-00 |
| 30 | 13 | 12 | 5 | 0.10906E-02 | 14 | 6 | 5 | 0.20949E-00 |
| 31 | 13 | 10 | 5 | 0.10348E-02 | 14 | 6 | 5 | 0.19761E-00 |
| 32 | 13 | 10 | 5 | 0.98559E-03 | 14 | 4 | 5 | 0.18647E-00 |
| 33 | 13 | 10 | 5 | 0.93741E-03 | 13 | 10 | 5 | 0.17718E-00 |
| 34 | 13 | 10 | 5 | 0.88986E-03 | 13 | 10 | 5 | 0.16825E-00 |
| 35 | 13 | 10 | 5 | 0.84269E-03 | 13 | 10 | 5 | 0.15943E-00 |
| 36 | 13 | 8 | 5 | 0.80066E-03 | 13 | 8 | 5 | 0.15081E-00 |
| 37 | 13 | 8 | 5 | 0.76280E-03 | 14 | 2 | 5 | 0.14395E-00 |
| 38 | 13 | 8 | 5 | 0.72497E-03 | 14 | 2 | 5 | 0.13753E-00 |
| 39 | 13 | 8 | 5 | 0.68784E-03 | 14 | 2 | 5 | 0.13113E-00 |
| 40 | 13 | 6 | 5 | 0.65276E-03 | 14 | 2 | 5 | 0.12473E-00 |
| 41 | 13 | 6 | 5 | 0.62291E-03 | 14 | 2 | 5 | 0.11837E-00 |
| 42 | 13 | 6 | 5 | 0.58298E-03 | 14 | 2 | 5 | 0.11215E-00 |
| 43 | 13 | 6 | 5 | 0.56300E-03 | 14 | 2 | 5 | 0.10613E-00 |
| 44 | 13 | 6 | 5 | 0.53342E-03 | 13 | 6 | 5 | 0.10045E-00 |
| 45 | 13 | 6 | 5 | 0.50441E-03 | 13 | 6 | 5 | 0.95024E-01 |
| 46 | 13 | 4 | 5 | 0.47925E-03 | 13 | 4 | 5 | 0.90282E-01 |
| 47 | 13 | 4 | 5 | 0.45563E-03 | 13 | 4 | 5 | 0.85837E-01 |
| 48 | 13 | 4 | 5 | 0.43239E-03 | 13 | 4 | 5 | 0.81466E-01 |
| 49 | 13 | 4 | 5 | 0.40948E-03 | 13 | 4 | 5 | 0.77159E-01 |
| 50 | 13 | 4 | 5 | 0.38680E-03 | 13 | 4 | 5 | 0.72900E-01 |
| 51 | 13 | 4 | 5 | 0.36450E-03 | 13 | 2 | 5 | 0.68741E-01 |
| 52 | 13 | 2 | 5 | 0.34414E-03 | 13 | 2 | 5 | 0.65095E-01 |
| 53 | 13 | 2 | 5 | 0.32527E-03 | 13 | 2 | 5 | 0.61525E-01 |

BOUNDARY LAYER ANALYSIS FOR REYNOLDS NO OF 0 205E.08

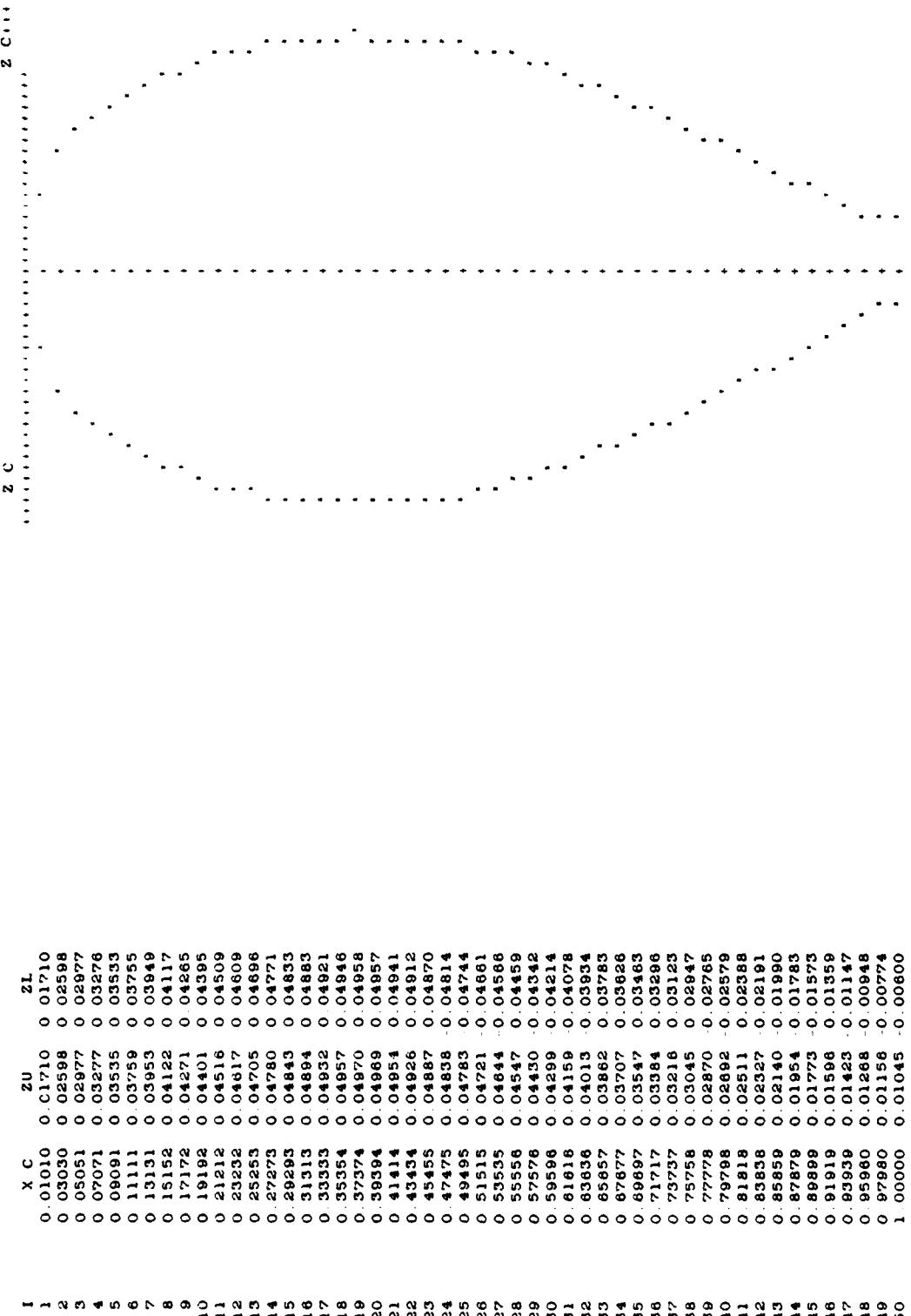
| X | Z | 2NEW | H | DELS | THETA | SEP | H | P1 | IND | TAU |
|---------|---------|----------|---------|---------|---------|---------|-----------|----------|------|---------|
| 0 07071 | 0 03271 | 0 032277 | 1 30845 | 0 00001 | 0 00001 | 0 00007 | 1 0 4530 | 0 16684 | 13 0 | 00186 |
| 0 09091 | 0 03524 | 0 03535 | 1 17866 | 0 00012 | 0 00006 | 0 00013 | 2 0 13480 | 0 13480 | 12 0 | 00161 |
| 0 11111 | 0 03741 | 0 03759 | 1 13413 | 0 00019 | 0 00010 | 0 00005 | 1 90857 | 0 02334 | 11 0 | 00154 |
| 0 13131 | 0 03929 | 0 03953 | 1 13903 | 0 00024 | 0 00013 | 0 00004 | 1 87177 | 0 06475 | 11 0 | 00148 |
| 0 15152 | 0 04093 | 0 04122 | 1 14959 | 0 00029 | 0 00016 | 0 00008 | 1 86620 | 0 05075 | 11 0 | 00143 |
| 0 17172 | 0 04238 | 0 04271 | 1 15635 | 0 00034 | 0 00018 | 0 00003 | 1 86117 | 0 03483 | 11 0 | 00138 |
| 0 19192 | 0 04362 | 0 04401 | 1 16024 | 0 00039 | 0 00021 | 0 00002 | 1 86456 | 0 03207 | 11 0 | 00134 |
| 0 21212 | 0 04472 | 0 04516 | 1 16354 | 0 00044 | 0 00024 | 0 00003 | 1 86153 | 0 04057 | 10 0 | 00132 |
| 0 23232 | 0 04568 | 0 04617 | 1 16680 | 0 00048 | 0 00028 | 0 00003 | 1 85837 | 0 05684 | 10 0 | 00130 |
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| 0 27273 | 0 04723 | 0 04780 | 1 17861 | 0 00057 | 0 00031 | 0 00006 | 1 85469 | 0 09782 | 10 0 | 00126 |
| 0 29293 | 0 04782 | 0 04843 | 1 18298 | 0 00061 | 0 00033 | 0 00007 | 1 85476 | 0 11918 | 10 0 | 00125 |
| 0 31313 | 0 04828 | 0 04894 | 1 19023 | 0 00065 | 0 00035 | 0 00008 | 1 85608 | 0 13871 | 10 0 | 00124 |
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| 0 35354 | 0 04884 | 0 04957 | 1 20647 | 0 00073 | 0 00039 | 0 00011 | 1 86245 | 0 16818 | 10 0 | 00122 |
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| 0 77778 | 0 02587 | 0 02870 | 0 85751 | 0 00279 | 0 00162 | 0 00099 | 1 72897 | 2 35111 | 11 0 | 00106 |
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| 0 91919 | 0 01068 | 0 01596 | 0 75551 | 0 00534 | 0 00242 | 0 00275 | 2 0 20735 | 54 92084 | 55 0 | 00015 |
| 0 93939 | 0 00821 | 0 01423 | 0 73594 | 0 00621 | 0 00268 | 0 00307 | 2 31573 | 22 15929 | 29 0 | 00028 |
| 0 95960 | 0 00571 | 0 01268 | 0 71711 | 0 00555 | 0 00290 | 0 00205 | 1 91248 | 2 96701 | 11 0 | 00168 |
| 0 97980 | 0 00321 | 0 01156 | 0 71048 | 0 00733 | 0 00299 | 0 00265 | 2 44948 | | 51 0 | 00000 |
| 1.00000 | 0.00070 | 0.01045 | 0.69042 | 0.01012 | 0.00339 | 0.00552 | 2.98649 | | 51 0 | 0.00000 |

INVERSE SHAPE AT $J = 12$

| | X C | ZU | ZL |
|-----|---------|---------|---------|
| 1 | 0.01010 | 0.01710 | 0.01710 |
| 1.1 | 0.03030 | 0.02598 | 0.02598 |
| 2 | 0.05051 | 0.02977 | 0.02977 |
| 3 | 0.07071 | 0.03246 | 0.03265 |
| 4 | 0.09091 | 0.03508 | 0.03527 |
| 5 | 0.11111 | 0.03748 | 0.03759 |
| 6 | 0.13131 | 0.03934 | 0.03951 |
| 7 | 0.15152 | 0.04091 | 0.04117 |
| 8 | 0.17172 | 0.04235 | 0.04265 |
| 9 | 0.19192 | 0.04363 | 0.04396 |
| 10 | 0.21212 | 0.04481 | 0.04510 |
| 11 | 0.23232 | 0.04595 | 0.04610 |
| 12 | 0.25253 | 0.04700 | 0.04697 |
| 13 | 0.27273 | 0.04802 | 0.04772 |
| 14 | 0.29293 | 0.04900 | 0.04834 |
| 15 | 0.31313 | 0.04995 | 0.04884 |
| 16 | 0.33333 | 0.05089 | 0.04922 |
| 17 | 0.35354 | 0.05182 | 0.04947 |
| 18 | 0.37374 | 0.05275 | 0.04960 |
| 19 | 0.39394 | 0.05369 | 0.04958 |
| 20 | 0.41414 | 0.05468 | 0.04943 |
| 21 | 0.43434 | 0.05566 | 0.04914 |
| 22 | 0.45455 | 0.05669 | 0.04872 |
| 23 | 0.47475 | 0.05766 | 0.04815 |
| 24 | 0.49495 | 0.05839 | 0.04745 |
| 25 | 0.51515 | 0.05884 | 0.04663 |
| 26 | 0.53535 | 0.05829 | 0.04568 |
| 27 | 0.55556 | 0.05744 | 0.04461 |
| 28 | 0.57576 | 0.05618 | 0.04344 |
| 29 | 0.59596 | 0.05483 | 0.04217 |
| 30 | 0.61616 | 0.05305 | 0.04081 |
| 31 | 0.63636 | 0.05158 | 0.03937 |
| 32 | 0.65657 | 0.05014 | 0.03786 |
| 33 | 0.67677 | 0.04887 | 0.03629 |
| 34 | 0.69697 | 0.04715 | 0.03467 |
| 35 | 0.71717 | 0.04557 | 0.03300 |
| 36 | 0.73737 | 0.04392 | 0.03128 |
| 37 | 0.75758 | 0.04219 | 0.02951 |
| 38 | 0.77778 | 0.04037 | 0.02771 |
| 39 | 0.79798 | 0.03845 | 0.02586 |
| 40 | 0.81818 | 0.03641 | 0.02396 |
| 41 | 0.83838 | 0.03424 | 0.02201 |
| 42 | 0.85859 | 0.03192 | 0.02003 |
| 43 | 0.87879 | 0.02944 | 0.01801 |
| 44 | 0.89899 | 0.02681 | 0.01597 |
| 45 | 0.91919 | 0.02405 | 0.01391 |
| 46 | 0.93939 | 0.02117 | 0.01192 |
| 47 | 0.95960 | 0.01825 | 0.01020 |
| 48 | 0.97980 | 0.01534 | 0.00891 |
| 49 | 1.00000 | 0.01275 | 0.00762 |

... PLOT OF NEW ORDINATES AFTER B L CALCULATION AND

SMOOTHING ..



SPAN STATION Eta 0 154
CLS 0 23271 CDS 0 00817 CMS 0 03419

| | X | C | CPU | CPL | RHOU | RHOI | MACHU | MACHL | CP..... | CP..... |
|----|---|-------|---------|---------|---------|---------|---------|---------|---------|---------|
| 1 | 0 | 01010 | 0 35162 | 0 41652 | 0 62767 | 0 82187 | 1 01187 | 0 63886 | 0 | 0 |
| 2 | 0 | 03030 | 0 74415 | 0 14369 | 0 51871 | 0 75523 | 1 22528 | 0 77086 | 0 | 0 |
| 3 | 0 | 05051 | 0 56910 | 0 08695 | 0 56833 | 0 74107 | 1 2808 | 0 79794 | 0 | 0 |
| 4 | 0 | 07071 | 0 43701 | 0 08451 | 0 80465 | 0 73545 | 1 05574 | 0 80865 | 0 | 0 |
| 5 | 0 | 09091 | 0 40424 | 0 03568 | 0 61353 | 0 72819 | 1 03878 | 0 82243 | 0 | 0 |
| 6 | 0 | 11111 | 0 40884 | 0 01036 | 0 61282 | 0 72179 | 1 04012 | 0 83454 | 0 | 0 |
| 7 | 0 | 13131 | 0 41089 | 0 01145 | 0 61173 | 0 71627 | 1 04221 | 0 84499 | 0 | 0 |
| 8 | 0 | 15152 | 0 41302 | 0 02985 | 0 61115 | 0 71159 | 1 04331 | 0 85381 | 0 | 0 |
| 9 | 0 | 17172 | 0 41497 | 0 04606 | 0 61063 | 0 70746 | 1 04432 | 0 86180 | 0 | 0 |
| 10 | 0 | 19192 | 0 41794 | 0 06110 | 0 60982 | 0 70362 | 1 04585 | 0 86883 | 0 | 0 |
| 11 | 0 | 21212 | 0 42281 | 0 07583 | 0 60850 | 0 69985 | 1 04837 | 0 87592 | 0 | 0 |
| 12 | 0 | 23232 | 0 42959 | 0 08055 | 0 60866 | 0 69807 | 1 05189 | 0 88302 | 0 | 0 |
| 13 | 0 | 25253 | 0 43831 | 0 10548 | 0 60430 | 0 69224 | 1 05642 | 0 89024 | 0 | 0 |
| 14 | 0 | 27273 | 0 44890 | 0 12071 | 0 60142 | 0 68831 | 1 06195 | 0 89762 | 0 | 0 |
| 15 | 0 | 29293 | 0 46113 | 0 13613 | 0 59809 | 0 68433 | 1 06834 | 0 90510 | 0 | 0 |
| 16 | 0 | 31313 | 0 47493 | 0 15170 | 0 59432 | 0 68030 | 1 07560 | 0 91267 | 0 | 0 |
| 17 | 0 | 33333 | 0 49000 | 0 16713 | 0 58019 | 0 67630 | 1 08356 | 0 92019 | 0 | 0 |
| 18 | 0 | 35354 | 0 50587 | 0 18199 | 0 58583 | 0 67243 | 1 09199 | 0 92745 | 0 | 0 |
| 19 | 0 | 37374 | 0 52259 | 0 19619 | 0 58122 | 0 66873 | 1 10092 | 0 93441 | 0 | 0 |
| 20 | 0 | 39394 | 0 53949 | 0 20892 | 0 57655 | 0 66541 | 1 11000 | 0 94066 | 0 | 0 |
| 21 | 0 | 41414 | 0 55500 | 0 21904 | 0 57225 | 0 66057 | 1 11839 | 0 94584 | 0 | 0 |
| 22 | 0 | 43434 | 0 56984 | 0 22739 | 0 56812 | 0 66057 | 1 12646 | 0 94975 | 0 | 0 |
| 23 | 0 | 45455 | 0 58485 | 0 23400 | 0 56394 | 0 65884 | 1 13468 | 0 95302 | 0 | 0 |
| 24 | 0 | 47475 | 0 59816 | 0 23694 | 0 56021 | 0 65807 | 1 14200 | 0 95447 | 0 | 0 |
| 25 | 0 | 49495 | 0 60856 | 0 23631 | 0 55730 | 0 65823 | 1 14776 | 0 95416 | 0 | 0 |
| 26 | 0 | 51515 | 0 61494 | 0 23286 | 0 55551 | 0 65914 | 1 15130 | 0 95245 | 0 | 0 |
| 27 | 0 | 53535 | 0 61482 | 0 22844 | 0 55554 | 0 66082 | 1 15123 | 0 94929 | 0 | 0 |
| 28 | 0 | 55556 | 0 60772 | 0 21773 | 0 55753 | 0 66057 | 1 14729 | 0 94474 | 0 | 0 |
| 29 | 0 | 57576 | 0 59133 | 0 20574 | 0 56213 | 0 66624 | 1 13824 | 0 93910 | 0 | 0 |
| 30 | 0 | 59596 | 0 53783 | 0 19286 | 0 57707 | 0 66985 | 1 10900 | 0 93268 | 0 | 0 |
| 31 | 0 | 61616 | 0 40489 | 0 17835 | 0 61335 | 0 67338 | 1 03912 | 0 92567 | 0 | 0 |
| 32 | 0 | 63636 | 0 26952 | 0 16930 | 0 64949 | 0 67731 | 0 91830 | 0 | 0 | 0 |
| 33 | 0 | 65657 | 0 21172 | 0 14780 | 0 66468 | 0 68131 | 0 94204 | 0 | 0 | 0 |
| 34 | 0 | 67677 | 0 18486 | 0 13220 | 0 87168 | 0 68535 | 0 92886 | 0 | 0 | 0 |
| 35 | 0 | 69697 | 0 15647 | 0 11686 | 0 67806 | 0 68937 | 0 91499 | 0 | 0 | 0 |
| 36 | 0 | 71717 | 0 12879 | 0 10114 | 0 68823 | 0 69335 | 0 90153 | 0 | 0 | 0 |
| 37 | 0 | 73737 | 0 10364 | 0 08579 | 0 69271 | 0 69729 | 0 88935 | 0 | 0 | 0 |
| 38 | 0 | 75758 | 0 08080 | 0 07015 | 0 69883 | 0 70130 | 0 87822 | 0 | 0 | 0 |
| 39 | 0 | 77778 | 0 05859 | 0 05402 | 0 70428 | 0 70543 | 0 86762 | 0 | 0 | 0 |
| 40 | 0 | 79798 | 0 03862 | 0 03715 | 0 70987 | 0 70973 | 0 85708 | 0 | 0 | 0 |
| 41 | 0 | 81818 | 0 01338 | 0 01868 | 0 71578 | 0 71443 | 0 84591 | 0 | 0 | 0 |
| 42 | 0 | 83838 | 0 01285 | 0 02020 | 0 72242 | 0 71988 | 0 83335 | 0 | 0 | 0 |
| 43 | 0 | 85858 | 0 04270 | 0 02501 | 0 72996 | 0 72550 | 0 81907 | 0 | 0 | 0 |
| 44 | 0 | 87879 | 0 07298 | 0 05019 | 0 73757 | 0 73185 | 0 80461 | 0 | 0 | 0 |
| 45 | 0 | 89899 | 0 10094 | 0 07920 | 0 74457 | 0 73913 | 0 79126 | 0 | 0 | 0 |
| 46 | 0 | 91919 | 0 13141 | 0 13145 | 0 75217 | 0 74801 | 0 77672 | 0 | 0 | 0 |
| 47 | 0 | 93939 | 0 17135 | 0 15520 | 0 76209 | 0 75809 | 0 75764 | 0 | 0 | 0 |
| 48 | 0 | 95950 | 0 20276 | 0 18597 | 0 76985 | 0 76570 | 0 74281 | 0 | 0 | 0 |
| 49 | 0 | 97990 | 0 21466 | 0 20521 | 0 77278 | 0 77045 | 0 73690 | 0 | 0 | 0 |
| 50 | 1 | 00000 | 0 25618 | 0 25222 | 0 78298 | 0 78201 | 0 71697 | 0 | 0 | 0 |

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1. South, J. C., Keller, J. D., and Hafez, M., "Vector Processor Algorithms for Transonic Flow Calculations," AIAA Journal, Vol. 18, No. 7, 1980 pp. 786-792.

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